# 6000 NEW HAMPSHIRE AVENUE WASHINGTON, DC PLANNED UNIT DEVELOPMENT 

STATEMENT<br>OF THE APPLICANTS<br>TO THE<br>DISTRICT OF COLUMBIA ZONING COMIMISSION<br>FOR A<br>CONSOLIDATED PLANNED UNIT DEVELOPMENT<br>AND<br>ZONING MAP AMENDMENT

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## PREFACE

This statement and attached documents are submitted by the WEST*GROUP Development Company LLC, and The Jarvis Company, LLC, the developers, on behalf of 6000 New Hampshire Avenue LLC, the owner of the subject property (collectively referred to herein as the "Applicants"), in support of their applications to the Zoning Commission of the District of Columbia for the consolidated review and one-step approval of a Planned Unit Development ("PUD") and related Zoning Map Amendment.

The property that is the subject of this application consists of Parcel 126/74, Lots 69, 70, 71, 72, 73, 801, 824 and 826 in Square 3714, and Lot 858 in Square 3719 (the "Subject Property"). The Subject Property is located in the northeast quadrant of the District. Parcel 126/74 and Lot 858 in Square 3719 are bounded by Rittenhouse Street, New Hampshire Avenue, Peabody Street, Chillum Place and Sligo Mill Road. Lots 70, 71, 72, 73, 801, 824 and 826 in Square 3714 are bounded by Peabody Street, New Hampshire Avenue, a 15 foot public alley, and $1^{\text {st }}$ Street. The Subject Property is currently zoned R-1-B, which permits a maximum height of forty feet and 3 stories. A maximum floor area ratio ("FAR") is not prescribed in the R-1-B District.

The Applicants are seeking consolidated PUD approval and rezoning of the Subject Property to the R-5-A District, and intend to construct to a residential development of 199 units containing approximately 417,802 square feet of gross floor area dedicated to residential uses, with approximately 27 detached single family dwellings, 111 townhomes and 61 condominium apartments, on the Subject

Property. The detached single family dwellings will have a height of approximately 35 feet above the first floor elevation. The townhomes will have a height of approximately 30 feet above the first floor elevation. The existing buildings to be converted into condominiums are approximately 40 feet in height above the first floor elevation. The project will have an overall floor area ratio ("FAR") of approximately 0.83 and will include approximately 381 off-street parking spaces.

As set forth below, this statement and the attachments meet the filing requirements for a PUD application under Chapter 24 of the District of Columbia Zoning Regulations.

## DEVELOPMENT TEAM

| Developer: | WEST*GROUP Development Company LLC 1600 Anderson Road McLean, VA 22102 |
| :---: | :---: |
| Developer: | The Jarvis Company, LLC 2600 Virginia Avenue, N.W., Suite 701 Washington, DC 20037 |
| Builder: | Linde Development Companies $7118^{\text {th }}$ Street, SE Washington DC 20003 |
| Master Planner: | Ferrell Madden Associates $1914^{\text {th }}$ Street, SE Washington DC 20003 |
| Architect: | Frank Lohsen McCrery Architects 1750 Pennsylvania Avenue, NW, Suite 810 Washington DC 20006 |
| Architect: | Eric Colbert \& Associates $7175^{\text {th }}$ Street, NW Washington DC 20001 |
| Civil Engineers: | Kimley-Horn and Associates, Inc. 13755 Sunrise Valley Drive, Suite 450 Herndon VA 20171 |
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| Exhibit | Description |
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| A | Architectural Plans and Drawings |
| B | Zoning Map |
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## I. INTRODUCTION

This statement and the attached documents support the applications of the WEST*GROUP Development Company LLC, and The Jarvis Company, LLC, the developers, on behalf of $\mathbf{6 0 0 0}$ New Hampshire Avenue LLC, the owner of the subject property (collectively referred to herein as the "Applicants"), to the Zoning Commission for the District of Columbia ("Commission") for the consolidated review and one-step approval of a Planned Unit Development ("PUD") and related Zoning Map Amendment. The Applicants are seeking PUD approval and rezoning of the Subject Property to the R-5-A District.

The property that is the subject of this application consists of Parcel 126/74, Lots 69, 70, 71, 72, 73, 801, 824 and 826 in Square 3714, and Lot 858 in Square 3719 (the "Subject Property"). The Subject Property is located in the northeast quadrant of the District. Parcel 126/74 and Lot 858 in Square 3719 are bounded by Rittenhouse Street, New Hampshire Avenue, Peabody Street, Chillum Place and Sligo Mill Road, N.E. Lots 69, 70, 71, 72, 73, 801, 824 and 826 in Square 3714 are bounded by Peabody Street, New Hampshire Avenue, a 15 foot public alley, and $1^{\text {st }}$ Street, N.E. The Subject Property is currently zoned R-1-B, which permits a maximum height of forty feet and three stories. A maximum floor area ratio ("FAR") is not prescribed in the R-1-B District. The Applicants are seeking consolidated PUD approval and rezoning of the Subject Property to the R-5-A District. The requested zoning change is fully consistent with the District of Columbia Comprehensive Plan
("Comprehensive Plan"), including the land use element which designates the Subject Property in the low density residential land use category.

## A. Summary of Project

The Applicants propose to construct a residential development of 199 units containing approximately 417,802 square feet of gross floor area dedicated to residential uses, with approximately 27 detached single family dwellings, 111 townhomes and 61 condominium apartments, on the Subject Property. The detached single family dwellings will have a height of approximately 35 feet above the first floor elevation. The townhomes will have a height of approximately 30 feet above the first floor elevation. The existing buildings to be converted into condominiums are approximately 40 feet in height above the first floor elevation. The project will have an overall floor area ratio ("FAR") of approximately 0.83 and will include approximately 381 off-street parking spaces.

## B. Background Information Regarding Applicants

The development team for this project includes the WEST*GROUP Development Company LLC and The Jarvis Company, LLC. WEST*GROUP is a full-service real estate development, construction, brokerage, and management organization with over four decades of experience in the D.C. metropolitan area. WEST*GROUP's experienced team of real estate professionals has developed more than 13 million square feet of quality office, retail, industrial and residential space. The firm specializes in distinctive
build-to-suit projects. WEST*GROUP maintains a strong commitment to innovation, integrity and an active involvement in the community.

The Jarvis Company, LLC, a District of Columbia limited liability company, is a certified local-small-disadvantaged business enterprise founded in 1999 by fifth-generation Washingtonians and long-time, active participants in the business, political, and local community life of the Washington, D.C. metropolitan area. The Jarvis Company, LLC currently provides development consulting and general advice, counsel and assistance to real estate projects and partners; government relations and community development work; and permit acquisition, zoning counsel and/or other development related work, on a project-by-project basis, on projects and opportunities in the District of Columbia, Maryland, Virginia, and nationwide. Currently, The Jarvis Company, LLC is a member of the respective development teams that are engaged in the redevelopment of the old Convention Center site and the historic Franklin School, and on the team that is developing the mixed-use project to construct Radio One's corporate headquarters in Shaw.

## II. PROJECT DESCRIPTION

## A. Site Location and Description

## 1. Site Description

The Subject Property consists of consists of Parcel 126/74, Lots 69, 70, 71, 72, 73, 801, 824 and 826 in Square 3714, and Lot 858 in Square 3719. The Subject Property contains approximately 501,691 square feet of land
area. ${ }^{1}$ The Subject Property is situated in Ward 4 near the District of Columbia and Maryland boundary line. The Generalized Land Use Map of the Comprehensive Plan designates the Subject Property in the low density residential land use category.

The Subject Property is currently improved with two vacant buildings that previously housed the Masonic and Eastern Star Nursing Home and Infirmary, but were most recently used as offices for Med-Star Health. The Applicants intend to convert these buildings into condominium apartment buildings. The use of these buildings as housing, as opposed to office uses, is more compatible with the surrounding residential uses and enhances the residential character of the neighborhood. The Applicants also propose to construct approximately 27 detached single family dwellings and 111 townhomes on the Subject Property.

## 2. Description of Surrounding Area

The Subject Property is located in the northeast quadrant of the District. The Subject Property is zoned R-1-B and is surrounded primarily by property also zoned R-1-B. The Comprehensive Plan designates the area to the north, east and south of the Subject Property in the low density
${ }^{1}$ The Applicants are discussing with two of the owners of single family dwellings adjacent to the larger parcel swapping land to even out the parcel. The plans submitted with the application, attached as Exhibit A, identify the locations of the areas to be exchanged. The Applicants will revise the plans to exclude those areas in the event that agreement cannot be reached with the two owners. If agreement is reached, those properties will be a part of the proposed development. For computational purposes, the land areas were adjusted to assume that the properties would be exchanged, which results in a slightly larger land area than is now included in the property.
residential land use category. The area to the west of the Subject Property is designated in the low density residential and production and technical employment land use categories.

## B. Project Design

The proposed PUD reflects the careful consideration given by the Applicants and the architects to the unique location of the Subject Property. The proposed PUD and requested rezoning are consistent with the surrounding uses and intensity of uses.

Careful consideration was given to the planning of the site. The goal was to develop the site in keeping with the best traditions of the neighborhoods of the District of Columbia. This proposal for new development is in keeping with, and complementary to, the surrounding neighborhoods. Townhouses are clustered at the core of the site and detached single family residences located at the perimeter. In this way, the existing detached single family houses across the street will face similar detached single family houses.

Green space is used to complement the homes, in the form of street trees and planting strips and also as clear, usable Civic Greens. These areas offer opportunities for play, relaxation, and community interaction. They are also used as locations for underground storm water remediation, eliminating the need for unsightly storm water retention ponds.

The new private streets are laid out to connect to the surrounding street system while at the same time to minimize traffic through the site,
encouraging safe speeds and providing on-street parking. Alleys are provided behind all units, allowing rear loaded garages, trash collection, and utility connections behind the units, rather than on the front.

The development was planned to be an appropriate and fitting example of Washingtonian residential architecture. A purposeful mix of unit types is employed, including condominium units of varying sizes; townhomes; and detached single family residences. Buildings are to be brick on all four sides, reflecting the homes in the surrounding neighborhoods. When complete, the new structures should blend seamlessly not only with each other, but also with the residences found in the neighboring communities.

The units have been designed with flexible layouts, to suit a wide range of family needs and sale prices. Each unit is provided with parking, most of which is off-street in garages. Porches and front stoops are pedestrian in scale, helping to establish a healthy sense of community and promote interaction between neighbors. Most units are also provided with a rear deck or balcony, encouraging interaction along the alleys. The net result is more eyes on the street, which will increase not only the sense of community but also the physical security of the neighborhood.

This project contains an extensive landscaping program. Street trees are to be planted in relatively close proximity, lining the streets with their trunks, and shading the walks and fronts of the houses with their canopies. Elm trees, which have been devastated by disease, are to be re-introduced in
the form of new, disease resistant cultivars such as the Liberty Elm. Red Maple trees surround the public green spaces, accenting them as special places with their dramatic foliage. Evergreen trees are used as screening elements, to contain undesirable views and provide privacy where appropriate.

## C. Matter of Right Development under Existing Zoning

The Subject Property is zoned R-1-B. The R-1 District is designed to protect quiet residential areas now developed with one-family detached dwellings and adjoining vacant areas likely to be developed for those purposes. 11 DCMR §200.1. The R-1 District is subdivided into R-1-A and R-1-B Districts, providing for districts of low and high density, respectively. 11 DCMR §200.3. The R-1-B District permits a maximum height of forty feet and three stories. 11 DCMR §400.1. Lots in the R-1-B District are required to have a minimum lot area of 5,000 square feet, and a minimum lot width of fifty feet. 11 DCMR §401.3 A maximum FAR is not prescribed in the R-1-B District. 11 DCMR §402.4 One-family detached dwellings are permitted in the R-1-B District pursuant to Section 201.1(b). 11 DCMR § 201.1(b). Parking is required at a rate of one parking space for each dwelling unit. 11 DCMR §2101.1. Under the PUD guidelines for the R-1-B District, the maximum permitted height for a residential use is forty feet, and the maximum FAR is 0.4. 11 DCMR §§ 2405.1, 2405.2.

## D. Matter of Right Development under Proposed Zoning

Under the proposed PUD, the zoning of the Subject Property would become R-5-A. The R-5 Districts are General Residence Districts designed to permit flexibility of design by permitting in a single district all types of urban residential development if they conform to the established height, density, and area requirements. 11 DCMR §350.1. The R-5-A District is designed to permit low height and density developments. 11 DCMR §350.2. The R-5-A District permits a maximum height of forty feet, with no limitation on the number of stories, and a maximum FAR of 0.9 for all structures. 11 DCMR §§400.1, 402.4. Parking in the R-5-A District is required at a rate of one space for each dwelling unit. 11 DCMR § 2101.1. Under the PUD standards for the R-5-A District, the maximum permissible height is sixty feet. 11 DCMR § 2405.1. The PUD standards for the R-5-A District permit a maximum FAR of 1.0 for residential uses. 11 DCMR § 2405.2.

## E. Tabulation of Development Data

See tabulation of development data on Sheets D01 and T01 of the Architectural Plans and Drawings attached hereto as ExhibitA.

## F. Flexibility under PUD Guidelines

The PUD process was created to allow greater flexibility in planning and design than may otherwise be possible under conventional zoning procedures. Thus, the Applicants seek flexibility from several provisions of the Zoning Regulations. As permitted under section 2405.8, the Commission may grant such flexibility without the need for special exception approval
from the Board of Zoning Adjustment or compliance with the special exception standards that might otherwise apply.

1. Flexibility Pursuant to Sections 410 and 2516 of the Zoning Regulations

Section 410.1 of the Zoning Regulations provides that in an R-5 District, if approved by the Board of Zoning Adjustment as a special exception, a group of one-family dwellings, flats, or apartment houses, or a combination of these buildings, with division walls erected from the ground up or from the lowest floor up, may be erected and deemed a single building for the purpose of the Zoning Regulations. 11 DCMR §410.1. Section 2516 of the Regulations allows multiple buildings on a single subdivided record lot, which is useful where as here, there are large deep lots having a smaller amount of street frontage.

As shown on the proposed site plan labeled as Sheet $S 01$ of the Architectural Plans and Drawings attached hereto as Exhibit A, the Applicants propose to erect the townhomes in groups of buildings. All buildings in the group of buildings will be erected simultaneously, and all front entrances of the group will abut either a street, front yard or front court. However, since the Subject Property has a large land area compared to the amount of street frontage, the Applicants propose that the Zoning Commission treat each grouping of townhomes as a single building for the purpose of the Zoning Regulations so that each individual dwelling need not satisfy all the area and bulk provisions.

## 2. Flexibility from Yard Requirements

Pursuant to Section 405.9 of the Zoning Regulations, side yards provided in the R-5-A District must have a minimum width of not less eight feet. A rear yard with a minimum width of twenty feet is also required 11 DCMR §404.1. For lots having no street frontage, a front yard equal to the minimum required rear yard is also required by $\S 2516.5(\mathrm{~b})$. The Applicants request flexibility from these requirements because a number of the yards provided are less than the required width. As shown on the Architectural Plans and Drawings attached hereto as Exhibit A, including the computations on Sheet T01, the Applicants have designed the layout of the proposed development to meet as many of the applicable zoning requirements as possible. However, due to design and massing features of the project, and the clustering of units to ensure open space, a number of the units do not have complying yards. However, the project includes a significant amount of open space, as the overall lot occupancy is approximately $29.4 \%$, and approximately $34.9 \%$ of the Subject Property is devoted to open, green space.
III.

THE PROJECT MEETS THE STANDARDS OF THE ZONING REGULATIONS AND PUD REQUIREMENTS

## A. PUD Process is Appropriate Mechanism for the Project

The PUD process is the appropriate mechanism for guiding the development of the PUD Site. It allows the project to be developed within the purview of the Zoning Commission while at the same time providing opportunities for input from various agencies and parties. Through the PUD
process, the Office of Planning and other District agencies will have the opportunity for greater participation in the fulfillment of the District's planning objectives for this area. Similarly, the adjacent property owners and area residents will have the opportunity to express their views about the proposed development. Accordingly, the use of the PUD process gives the community and District agencies an opportunity to work with the Applicants to ensure a well-planned development.

## B. PUD Requirements under Chapter 24 of the Zoning Regulations

## 1. Area Requirements under Section 2402.1(c)

The PUD Site area is approximately 501,691 square feet (approximately 11.5 acres) in land area, which exceeds the minimum area requirement of two acres for a PUD in the R-5-A District. 11 DCMR §2401.1(b).

## 2. Height and FAR Requirements under Sections 2405.1 and 2405.2

The proposed development has been evaluated under the PUD guidelines for the R-5-A District. As noted above, under the PUD guidelines for the R-5-A District, the maximum height of the project is limited to 60 feet. 11 DCMR §2405.1. The maximum FAR for a PUD in the R-5-A District is 1.0 for residential uses. 11 DCMR § 2405.2. The detached single family dwellings will have a height of approximately 35 feet above the first floor elevation. The townhomes will have a height of approximately 30 feet above the first floor elevation. The existing buildings to the converted into
condominiums are approximately 40 feet in height above the first floor elevation. These heights are less than the permissible height. Moreover, the project will have a residential FAR of 0.83 , or 417,802 square feet of gross floor area, which is less than the maximum permitted as a matter-of-right or under the PUD guidelines.

## 3. Impacts of the Project under Section 2403.3

The proposed PUD will have a positive impact on the surrounding area. Overall, the proposed development will significantly improve the existing area by virtue of the exceptional architectural design, as well as by providing development to a currently underdeveloped site. The proposed PUD's design carefully considers the nearby residences and accordingly, will have a minimal impact on that area.

The proposed PUD will have no unacceptable impact on traffic. As indicated in the traffic impact study, attached hereto as Exhibit F, the proposed development will have no effect on the intersection levels of service and they will continue to operate at levels of service A and B. The traffic impact study also indicates that the area is well served by transit and that pedestrian connections in the area will be enhanced by the development. The traffic impact analysis also concludes that the amount of proposed parking spaces satisfies both the Zoning Requirements and the practical requirements of the development, and as a result, there will be no spillover parking into the surrounding community.

## 4. Not Inconsistent with Comprehensive Plan under Section 2403.4

As discussed at length below, the PUD project is not inconsistent with the Comprehensive Plan, as discussed at length below.

## C. Goals and Objectives of the Proposed PUD

The proposed PUD is designed to achieve several important goals and objectives, as discussed below.

## D. Public Benefits and Project Amenities

## 1. Overview

The PUD guidelines require the evaluation of specific public benefits and project amenities for a proposed project. Public benefits are defined as "superior features of a proposed planned unit development that benefit the surrounding neighborhood or the public in general to a significantly greater extent than would likely result from the development of the site under the matter of right provisions...." 11 DCMR 2403.6. A project amenity is further defined as "one type of public benefit, specifically a functional or aesthetic feature of the proposed development, that adds attractiveness, convenience or comfort of the project for occupants and immediate neighbors." 11 DCMR 2403.7. Additionally, when deliberating the merits of a PUD application, the Zoning Commission is required to "judge, balance and reconcile the relative value of the project amenities and public benefits offered, the degree of development incentives requested, and any potential adverse effects according to the specific circumstances of the case." 11 DCMR 2403.8. Public
benefits and project amenities may be exhibited in a variety of ways and may overlap with furthering the policies and goals of the Comprehensive Plan.

## 2. Housing and Affordable Housing (Section 2403.9(f))

The single greatest benefit to the area, and the city as a whole, is the creation of new housing consistent with the goals of the Zoning Regulations, the Comprehensive Plan and the Mayor's housing initiative. The proposed PUD will contain approximately 417,802 square feet of gross floor area dedicated to residential uses. The Applicants intend to convert the two vacant buildings on the Subject Property that previously housed the Masonic and Eastern Star Nursing Home and Infirmary, but were most recently used as offices for Med-Star Health, into condominium buildings. The use of these buildings as housing, as opposed to office uses, is more compatible with the surrounding residential uses and enhances the residential character of the neighborhood. Moreover, the Applicants are committed to ensuring that people with low and moderate incomes share the homes and benefits to be provided by the proposed PUD. Therefore, the project will include 10 units offered as affordable housing units. Five of the affordable units will be townhomes and five will be condominium units. The affordable units will be integrated throughout the development. Eligible purchasers will be families and individuals whose annual incomes are no more than $80 \%$ of the area median income.

The West condominium building will also be restricted to residency by persons aged fifty-five and older. This will offer the possibility that senior
citizens residing in the community could remain in the community in a smaller, more maintenance friendly home. This building will be designed to be handicapped accessible and will contain additional features to facilitate an independent lifestyle for the residents.

## 3. Urban Design, Architecture, Landscaping and Open Space (Section 2403.9(a))

The high quality of architectural design in the proposed development exceeds that of most matter of right projects. The Applicants have commissioned the exceptional architectural design firms of Ferrell Madden Associates, Frank Lohsen McCrery Architects and Eric Colbert \& Associates to create buildings that will further the goals of urban design and enhance the streetscape and surrounding neighborhood.

The project has an overall lot occupancy of $29.4 \%$. This is $10.6 \%$ less than the matter-of-right lot occupancy of $40 \%$ in both the R-1-B and R-5-A Districts. The open spaces are distributed throughout the site, and include Civic Greens that serve as common open focal space.

As noted earlier, this project contains an extensive landscaping program. Street trees are to be planted in relatively close proximity, lining the streets with their trunks, and shading the walks and fronts of the houses with their canopies. Elm trees, which have been devastated by disease, are to be re-introduced in the form of new, disease resistant cultivars such as the Liberty Elm. Red Maple trees surround the public green spaces, accenting them as special places with their dramatic foliage. Evergreen trees are used
as screening elements, to contain undesirable views and provide privacy where appropriate.
4. First Source Employment Agreement and Local, Small and ... Disadvantaged Business Enterprises (Section 2403.9(j))

Expanding employment opportunities for residents and local businesses is a priority of the Applicants. Indeed, The Jarvis Company, LLC, is a certified LSDBE and has substantial experience in outreach to disadvantaged businesses and a proven track record in working with communities to maximize economic and employment opportunities during development. Moreover, the Applicants will be entering a First Source Employment Agreement with the Department of Employment Services. The Applicants will also be entering a Local, Small, and Disadvantaged Business Enterprises (LSDBE) Memorandum of Understanding with the District's Office of Local Business Development.

## IV. COMPLIANCEE WITH THE COMPREHENSIVE PLAN

The proposed PUD advances the purposes of the Comprehensive Plan, is consistent with the Generalized Land Use Map, and furthers and complies with the major themes and elements for the District and Ward 4 in the Comprehensive Plan.

## A. Purposes of the Comprehensive Plan

The purposes of the Comprehensive Plan are six-fold:
(1) Define the requirements and aspirations of District residents, and accordingly influence social, economic and physical development; (2) Guide executive and legislative decisions on matters affecting the District and its citizens; (3) Promote economic growth and jobs for District residents; (4) Guide private and public development in order to achieve District and community goals; (5) Maintain and enhance the natural and architectural assets of the District; and (6) Assist in conservation, stabilization, and improvement of each neighborhood and community in the District.
D.C. Code §1-245(b).

The PUD project significantly advances these purposes by promoting the social, physical and economic development of the District through the provision of a quality residential development that is affordable to a range of incomes; and the replacement of a primarily unimproved property with development that will enhance the built environment.

## B. Generalized Land Use Map

The proposed rezoning is consistent with the Generalized Land Use Map, which designates the Subject Property in the low density residential land use category. The project will have an overall FAR of approximately 0.83 , which is below the effective density of 1.2 FAR ( $40 \%$ lot occupancy times three stories) permitted in the R-1-B District. The number of units proposed is approximately seventeen units per acre. The R-1-B, District permits approximately 8.5 units per acre, the R-2 District permits approximately
fourteen units per acre and the R-3 District permits approximately twentytwo units per acre. The proposed development is therefore within the limits of the range of single-family zones.

Further, the overall density of the broad swath designated for low density residential along the northeastern boundary of the District would remain essentially unchanged. Since the Generalized Land Use Map does not drill down to establish the density permitted on each site, the Zoning Commission can appropriately increase the density on a particular site as long as the overall character and density are maintained. The Subject Property is the only large underdeveloped residential site in this area. Allowing the density proposed with the clustered site plan will result in a variety of housing types to hit different segments of the local housing market, consistent with other policies of the Comprehensive Plan discussed below.

## C. Compliance with Major Themes of the Comprehensive Plan

The Project is consistent with many of the Comprehensive Plan's major themes as follows:

1. Stabilizing and Improving the District's Neighborhoods

The proposed PUD will significantly increase the availability and variety of housing in the District. Moreover, the proposed residential use will create a stable and vibrant neighborhood. Finally, the inclusion of a number of affordable housing units will increase housing opportunities in Ward 4 and the District.

## 2. Increasing the Quantity and Quality of Employment Opportunities in the District

The Applicants are committed to expanding employment opportunities for residents, and will be entering both a First Source Employment Agreement with the Department of Employment Services and a Local, Small, and Disadvantaged Business Enterprises (LSDBE) Memorandum of Understanding with the District's Office of Local Business Development.

## 3. Respecting and Improving the Physical Character of the District

The Applicants' proposal respects and improves the physical character of the District through the construction of a well-planned and carefully designed development that provides a mix of housing types and includes affordable housing units.
4. Reaffirming and Strengthening the District's Role as an Economic Hub

The Comprehensive Plan encourages maximum use of the District's location for both private and public growth to promote economic development. Housing construction for all income levels is paramount to the success of the economic goals of the District. This mixed-income, mixed-housing type project furthers this theme by incorporating residential development to promote the economic health and well-being of the region.

## D. Compliance with Major Elements of the Comprehensive Plan

The proposed PUD furthers the objectives and policies of many of the Comprehensive Plan's major elements as follows:

## 1. Housing Element

According to the Housing element of the Comprehensive Plan, housing in the District is viewed as a key part of a total urban living system that includes access to transportation and shopping centers, the availability of employment and training for süitable employment, neighborhood schools, libraries, recreational facilities, playgrounds, and other public amenities. See 10 DCMR § 300.4. Also as stated in the Housing element of the Comprehensive Plan, the District recognizes its obligation to facilitate the availability of adequate, affordable housing to meet the needs of current and future residents. The District strives to stimulate a wider range of housing choices and strategies through the production of new units for a variety of household types. A priority under the District's housing element of the Comprehensive Plan is to maintain and upgrade the District's affordable rental stock, a goal that is supported by the proposed PUD. See 10 DCMR §§ 300.1-300.3.

The proposed PUD meets this goal by providing a total of approximately 417,802 square feet of gross floor area dedicated to residential uses. Moreover, the Applicants are committed to ensuring that people with low and moderate incomes share the homes and benefits to be provided by
the proposed PUD. Therefore, the project will include 10 units offered as affordable housing units. Five of the affordable units will be townhomes and five will be condominium units. The affordable units will be integrated throughout the development. Eligible purchasers will be families and individuals whose annual incomes are no more than $80 \%$ of the area median income.

## 2. Urban Design Element

The Urban Design element states that it is the District's goal to promote the protection, enhancement and enjoyment of the natural environs and to promote a built environment that serves as a complement to the natural environment, provides visual orientation, enhances the District's aesthetic qualities, emphasizes neighborhood identities, and is functionally efficient. See 10 DCMR § 701.1.

The Urban Design element also has an objective of encouraging new construction or renovation/rehabilitation of older buildings in areas with vacant or underused land or structures in order to create a strong, positive physical identity. See 10 DCMR § 712.1.

The proposed PUD has been designed to enhance the physical character of the area and complement the materials, height, scale and massing of the surrounding development. See 10 DCMR § 708.2.

The streetscape objective of this element is to establish a clear classification of streets and sidewalks that is functionally efficient and visually coherent, enhances the pedestrian environment, and provides for the
orderly movement of goods and services. See 10 DCMR § 709.1. The new private streets are laid out to minimize traffic through the site, encouraging safe speeds and providing on-street parking. Alleys are provided behind all units, allowing rear loaded garages, trash collection, and utility connections behind the units, rather than on the front.

## 3. Land Use Element

The Land Use element encourages a substantial amount of new housing in order for the District to perform its role as the region's urban center providing the greatest density of jobs and housing. 10 DCMR § 1100.2. Policies designed to support residential neighborhoods include promoting the enhancement and revitalization of District neighborhoods for housing and related uses; ensuring a broad range of residential neighborhood options, and providing wide-ranging assistance for neighborhoods for relatively poor quality by joint public and private action and concentrated governmental attention and resources. 10 DCMR §§ 1104.1 (a), (c), and (e), and 1118.6. The proposed PUD responds to these goals with the development of a highquality residential project that includes housing opportunities for a range of incomes.
E. Compliance with Ward 4 Elements of the Comprehensive Plan

1. Ward 4 Housing Element

A primary objective for housing in Ward 4 is to provide for the housing needs of low- and moderate-income households, and the Ward 4 housing
element calls for stimulating new and rehabilitated housing to meets all levels of need and demand. 10 DCMR $\S \S 1508.1$ (a), 1509.1(a). The proposed PUD will contain a total of approximately 417,802 square feet of gross floor area dedicated to residential uses. Moreover, the Applicants are committed to ensuring that people with low and moderate incomes share the homes and benefits to be provided by the proposed PÜD. Therefore, the project will include 10 units offered as affordable housing units. Five of the affordable units will be townhomes and five will be condominium units. The affordable units will be integrated throughout the development. Eligible purchasers will be families and individuals whose annual incomes are no more than $80 \%$ of the area median income.

## 2. Ward 4 Transportation Element

An objective for transportation in Ward 4 is to support the living environment and commerce of the ward and the District and to support development objectives for expanded housing opportunities for ward residents. 10 DCMR § 1514.1 (a). Moreover, one of the policies in support of transportation is to continue to require developers to provide appropriate traffic studies and mitigation measures prior to major development. 10 DCMR § 1515.1(a), (2), (D).

The Applicants have submitted a Traffic Impact Study, which is attached hereto as Exhibit $F$, in connection with this application. As indicated in the study, the proposed development will have no effect on the intersection levels of service and they will continue to operate at levels of
service A and B. The traffic impact study also indicates that the area is well served by transit and that pedestrian connections in the area will be enhanced by the development. The traffic impact analysis also concludes that the amount of proposed parking spaces satisfies both the Zoning Requirements and the practical requirements of the development, and as a result, there will be no spillover parking into the surrounding community.

## 3. Ward 4 Urban Design Element

The objectives for urban design in Ward 4 include preserving and enhancing the physical qualities and character of the ward's neighborhoods through preservation and enhancement of its built environment, and encouraging well-designed developments in areas that are vacant, underused or deteriorated. 10 DCMR §§ 1520.1(a), (b). The Applicants has commissioned the architectural design firms of Ferrell Madden Associates, Frank Lohsen McCrery Architects and Eric Colbert \& Associates to create impressive buildings that will further the goals of urban design and enhance the streetscape and surrounding neighborhood. The development was planned to be an appropriate and fitting example of Washingtonian residential architecture. A purposeful mix of unit types is employed, including condominium units of varying sizes; townhomes; and detached single family residences. All are to be brick on all four sides, reflecting the homes in the surrounding neighborhoods. When complete, the new structures should blend seamlessly not only with each other, but also with the residences found in the neighboring communities.

## 4. Ward 4 Land Use Element

A key land use concern in Ward 4 is preserving, protecting, and stabilizing the ward's residential neighborhoods. §§ 1528.11(a), 1529.1(a). The proposed PUD responds to these goals with the development of a highquality project that includes housing opportunities for a range of incomes.

## V. <br> CONCLUSION

For the reasons stated above, the Applicants submit that the PUD and related map amendment meet the standards of Chapter 24 of the Zoning Regulations and are consistent with the purposes and intent of the Zoning Regulations and Zoning Map. Accordingly, the Applicants request that the Zoning Commission determine that the applications have merit and that a public hearing on the applications should be scheduled.

Respectfully submitted:
HOLLAND \& KNIGHT LLP

By:


By: $\quad$ tt \&. M
Steven E. Sher, Director of Zoning and Land Use Services

By:


2099 Pennsylvania Ave., N.W.
Suite 100
Washington, D.C. 20006
(202) 955-3000

## Exhibit A

## Architectural Plans and Drawings

## Submitted as Separate Attachments




## Wemingaon, C.C., Sequantrer 8, 2000 <br>  <br>  <br>  <br> 



## DISTRICT OF COLUMBIA GOVERNMENT OFFICE OF THE SURVEYOR

Washington, D.C., September 3, 2005
Plat for Building Permit of SQUARE 3714 LOT's $69,70,71,72,73,801,824,826$

Scale: 1 inch $=30$ feet | Recorded in Book 49 Page 2 (LOTS 69-73) |
| ---: |
| Book ART Page 785 (LOTS 801 |

| Recelpt No. |
| :--- |
| Furmished to: |$\quad 22418$

HOLLAND \& KNIGHT - FREDA

I heraby cestify that all existing inmpovements shown hereon, are completaly dimenstoned
 coversd porches, afe correctiy dimmensioned and phatted and agree witr phans accompanying accurataly to the same scate at the property lies shown on thls patand that by reasen of the proposed improvements to be erected as stown hareor the stece of any adifoting itito prembses is not ctecreased to an area less than is required by the Zontrog Regulations for ight prembses is not decreased to an ancal less than is requined by the Zomitrg Regulations tor ight and ventiation; and it is furthor corifitad and agreed that accassible parking ares where




 permits a maximum diveway grade of $12 \%$ across the pubilic parding and the pivats restricted property.)

Date: $\qquad$
Surveyor, D.C.
By:




Traffic Impact Study

## 6000 New Hampshire Avenue PUD Washington, D.C.

Prepared for: 6000 New Hampshire Avenue, LLC

This document, together with the concepts and designs presented herein, as an instrument of service, is intended only for the specific purpose and client for which it was prepared. Reuse of and improper reliance on this document without written authorization and adaptation by KimleyHorn and Associates, Inc. shall be without liability to Kimley-Horn and Associates, Inc.

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## INTRODUCTION

This report presents the results of a traffic impact study for the proposed 6000 New Hampshire Avenue development in northeast Washington, D.C. The site is located along the west side of New Hampshire Avenue between Peabody Street and Rittenhouse Street. It is bordered by New Hampshire Avenue to the east, Sligo Mill Road to the west, Peabody Street to the south, and Rittenhouse Street to the north. Included in this site is also a parcel in between New Hampshire Avenue and First Street, south of Peabody Street. The total site location is shown on Figure 1. The proposed development includes approximately 199 residential units, involving a mix of single family detached houses, townhouses, and condominiums. The site currently contains offices for Medstar Health and a vacant nursing home facility.

The following traffic study was prepared to satisfy the traffic requirements associated with the Planned Unit Development (PUD) application and in accordance with the direction provided by the District of Columbia Department of Transportation (DDOT).

The following sections of this report describe the area transportation system, existing traffic volumes, the calculation of background traffic volumes, and the impact of the proposed development.


Map Source:
ADC The Map
People,
Permit Auth.
No.: 20410152

## AREA TRANSPORTATION SYSTEM

## Existing Area Streets

Streets considered in this study included New Hampshire Avenue, a key arterial, which traverses the immediate site area, as well as other collector and neighborhood streets. A brief description of the area street system follows:

New Hampshire Avenue - This major north-south arterial serves as a major commuter route between Maryland and Washington, D:C. In the vicinity of the site, New Hampshire Avenue has a four-lane cross-section with sidewalks on both the east and west sides. It forms the eastern boundary of the property. The study intersections of New Hampshire Avenue with Rittenhouse Street and Peabody Street are signalized. The study intersection of New Hampshire Avenue and Quackenbos Street is unsignalized, with the Quackenbos Street approach being stop controlled.

Rittenhouse Street - This local east-west street, which forms the northern boundary of the study area, has a two-lane cross section with on-street parking and sidewalks on both the north and south sides in the vicinity of the site. To the west of Sligo Mill Road, Rittenhouse Street operates one-way westbound only and has a one-lane cross section. The study intersection of Rittenhouse Street and Sligo Mill Road is unsignalized, with all approaches being stop controlled.

Sligo Mill Road - This local north-south street extends northward from Chillum Place. In the vicinity of the site, Sligo Mill Road has a two-lane cross section with on-street parking and a sidewalk on the west side. It forms the western boundary of the study area. The study intersection of Sligo Mill Road with Chillum Place is unsignalized, with the Sligo Mill Road approach being stop controlled

Chillum Place - This local east-west street begins at Peabody Street and provides access to locations northwest of the study area. In the vicinity of the site, Chillum Place has a two-lane cross-section.

Peabody Street - This local east-west street extends eastward from Chillum Place. In the vicinity of the site, Peabody Street has a two-lane cross section. A sidewalk is provided along the north side in between the existing driveway serving the property and New Hampshire Avenue. Peabody Street and Chillum Place form the southern boundary of the study area. The study
intersection of Peabody Street with First Street is unsignalized, with the First Street approach being stop controlled. The study intersection of Peabody Street with New Hampshire Avenue is signalized.

First Street - This local east-west street intersects with Peabody Street at the location of the existing driveway that serves the property. First Street has a two lane cross section, and its intersection with Peabody Street is unsignalized, with the First Street approach being stop controlled.

Quackenbos Street-This local east-west roadway begins at New Hampshire Avenue and provides access to communities east of New Hampshire Avenue. It has a two lane cross section in the vicinity of the site and has sidewalks on both the north and south sides.

## Existing Area Transit Service

Existing transit service in the study area includes the nearby Fort Totten Metrorail station on the Red Line and Green Line, as well as Metrobus service.

Metrobus service in the vicinity of the study area is provided along New Hampshire Avenue by the New Hampshire Avenue-Maryland Line (Route K6). The New Hampshire Avenue-Maryland Line serves the White Oak, Northwest Park, Langley Park, Chillum, and Fort Totten Metrorail Station areas. The buses on this route travel north and south along New Hampshire Avenue on weekdays, weekends, and holidays.

There are six bus stops along New Hampshire Avenue in the study area, with three each on the northbound and southbound sides. Two of the southbound bus stops have bus shelters. One shelter is located near the intersection of New Hampshire Avenue and Rittenhouse Street, and the other is located near the intersection of New Hampshire Avenue and Peabody Street.

## Future Transportation Improvements

There are no programmed transportation improvements that were considered for this study.

## DESCRIPTION OF PROPOSED DEVELOPMENT

## Location

The proposed 6000 New Hampshire Avenue residential development is bordered by New Hampshire Avenue to the east, Sligo Mill Road to the west, Rittenhouse Street to the north, and Peabody Street to the south. Included in this site is also a parcel in between New Hampshire Avenue and First Street, south of Peabody Street. The proposed development consists of 199 residential units, including 27 single family detached homes and 172 multifamily units (townhouses and condominiums). The site currently contains offices for Medstar Health and a vacated nursing home. The property currently has seven vehicle access driveways, including one along Peabody Street opposite First Street, four along Sligo Mill Road, one along New Hampshire Avenue, and one on First Street.

## Vehicle Access

Vehicle access is planned to be provided along New Hampshire Avenue opposite Quackenbos Street, at three locations along Peabody Street including the existing driveway opposite First Street, at three driveways along Sligo Mill Road, and at one driveway along Rittenhouse Street. The presence of eight access points to serve 6000 New Hampshire Avenue will result in an effective dispersal of site traffic and the realignment of the existing driveway on New Hampshire Avenue will consolidate two intersections into one. The locations of the existing and proposed driveways are shown on Figure 2.

## Parking

The proposed site will include a total of 381 parking spaces. Of these, 280 spaces are provided specifically for the single family detached homes and multifamily units. This exceeds the zoning requirement of 199 parking spaces ( 1 space per residential unit). These spaces are strategically located to satisfy the needs of the individual residential units. In addition to these 280 spaces, an additional 101 private street parking spaces are also included within the property. The resulting 381 parking spaces will be more than sufficient to satisfy the parking needs for the 199 residential units with no resulting spillover of parking into the surrounding community.


## TRAFFIC VOLUMES

Traffic volumes used in this study include existing traffic volumes, the projection of traffic volumes to obtain background traffic volumes, and traffic generated by the proposed development to obtain total future traffic volumes. The District of Columbia transportation staff directed that the weekday AM and PM commuter peak hours be studied. Intersections identified for study by District of Columbia Department of Transportation staff are as follows:

- Sligo Mill Road and Rittenhouse Street
- Sligo Mill Road and Chillum Place
- First Street and Peabody Street
- New Hampshire Avenue and Peabody Street
- New Hampshire Avenue and Quackenbos Street
- New Hampshire Avemue and Rittenhouse Street and $3^{\text {rd }}$. Street

Figure 3 shows the lane designations at the study area intersections. The following sections describe the traffic volumes used in this study.

## Existing Traffic Volumes

Traffic counts were conducted at the study area intersections before schools closed in May 2005 between 7:00 AM and 9:00 AM and between 4:00 PM and 6:00 PM. These counts were used to establish current peak hour traffic conditions. The peak hours at each intersection were established by identifying the peak 60 minutes of traffic during the AM and PM peak hours. From these traffic counts, the peak study hours were identified for each intersection as follows:

- Sligo Mill Road and Rittenhouse Street - 7:30 to 8:30 AM, 5:00 to 6:00 PM
- Sligo Mill Road and Chillum Place - 7:45 to 8:45 AM, 4:30 to 5:30 PM
- First Street and Peabody Street - 7:15 to 8:15 AM, 5:00 to 6:00 PM
- New Hampshire Avenue and Peabody Street - 7:15 to 8:15 AM, 4:15 to 5:15 PM
- New Hampshire Avenue and Quackenbos Street - 7:00 to 8:00 AM, 5:00 to 6:00 PM
- New Hampshire Avenue and Rittenhouse Street and $3^{\text {rd }}$ Street- 7:15 to 8:15 AM, 5:00 to 6:00 PM

The existing peak hour traffic volumes at the study intersections are shown on Figure 4. The appendix of this report contains the traffic count and pedestrian count summaries. In addition to peak hour volumes, available average annual weekday traffic (AAWT) volumes for streets within
the study area were obtained from the District of Columbia Department of Transportation. These counts were taken by the District along Rittenhouse Street and New Hampshire Avenụe. For these streets, AAWT volumes are 5,400 and 28,800 vehicles, respectively, and are shown on Figure 4.



## Background Traffic Volumes

Background traffic volumes represent future traffic that would travel through the area intersections without the proposed 6000 New Hampshire Avenue development. In order to represent the growth of traffic resulting from development activity outside the study area, traffic volumes for each of the movements at the study intersections were increased by $1 \%$ per year to the horizon year of 2009, as directed by DDOT. These volumes are referred to as 2009 Background Traffic Volumes and are shown at the study intersections on Figure 5.

## Site Generated Traffic Volumes

Peak hour traffic volumes generated by the proposed residential development were calculated using the ITE Trip Generation Report based on trip equations for Land Use Codes 210 (singlefamily detached housing) and 204 (residential condominium/townhouse). A summary of the trip figures is shown in Table 1.

| Table 1 <br> 6000 New Hampshire Avenue <br> Site Generated Traffic Volumes |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | In | Out | Total | In | Out | Total |
| AM Peak Hour | PM Peak Hour |  |  |  |  |  |
| 172 Condo/Townhome <br> Residential Units | 14 | 66 | 80 | 63 | 31 | 94 |
| 27 Detached Single-Family <br> Homes | 7 | 21 | 28 | 21 | 12 | 33 |
| Total | 21 | 87 | 108 | 83 | 43 | 126 |

The AM and PM peak hour trips were assigned to the area streets based upon existing traffic volume patterns in the study area as well as the location of the site access points serving the proposed development along New Hampshire Avenue, Peabody Street, and Sligo Mill Road. The resulting percent distributions of site generated trips onto the key streets are listed below in Table 2. Trips were assigned to the site driveways based on two assumptions: (1) vehicles will tend to use the most convenient driveway, and (2) vehicles will tend to avoid using driveways at intersections with relatively high traffic volumes.


| Table 2  <br> Distribution of Site Generated Traffic To/From  |  |
| :--- | :---: |
|  | Residential Development |
| To/From North on New Hampshire Avenue | $25 \%$ |
| To/From South on New Hampshire Avenue | $50 \%$ |
| To/From West on Chillum Place | $12 \%$ |
| To/From East on Peabody Street | $4 \%$ |
| To/From West on Rittenhouse Street | $3 \%$ |
| To/From East on Rittenhouse Street | $2 \%$ |
| To/From East on Quackenbos Street | $1 \%$ |
| To/From South on First Street | $1 \%$ |
| To/From South on 3rd Street | $2 \%$ |

The assignment of site generated trips is shown on Figure 6.

## Total Future Traffic Volumes

Total future traffic volumes represent future traffic volumes with the proposed 6000 New Hampshire Avenue development in place. These volumes were calculated by adding the site generated trips (shown on Figure 6) to the background traffic volumes. The resulting total future peak hour traffic volumes are shown on Figure 7.

Total traffic volumes at site driveways were calculated using the traffic generated by the proposed 6000 New Hampshire Avenue residential development. The resulting driveway volumes are also shown on Figure 7. It should be noted that the existing trips to the Medstar offices were conservatively not subtracted from the site generated trips.



## ASSESSMENT OF TRAFFIC CONDITIONS

The following is a discussion of the assessment of traffic conditions.

## Intersection Capacity Analyses

Intersection capacity analyses were conducted for existing, background, and total future traffic volumes. The capacity analyses were conducted using Synchro Software Package, which utilizes methodologies in the Highway Capacity Manual ( 2000 Edition) for signalized and unsignalized intersections. The analyses of existing, background, and total future traffic volumes were based on the existing lane uses and operations at the study area intersections.

The results of the capacity analyses are summarized in Tables 3 and 4 for the study area intersections and proposed driveways, respectively. Analysis results show overall level of service and delay information for each intersection for the existing, background, and total future traffic volumes. The Synchro analysis worksheets are contained in the Appendix.

| INTERSECTION | Existing 2005 Conditions |  | 2009 BackgroundConditions |  | 2009 Total Future Conditions |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AM | PM | AM | PM | AM | PM |
| Sligo Mill Road and Rittenhouse Street (Unsignalized) | A (7.9) | A(7.1) | A (8.0) | A (7.1) | A (8.0) | A (7.2) |
| Sligo Mill Road and Chillum Place (Unsignalized) | A (0.9) | A (1.6) | A (0.9) | A (1.6) | A (1.2) | A (1.7) |
| First Street and Peabody Street (Unsignalized) | A (0.7) | A (0.8) | A (0.7) | A (0.8) | A (1.1) | A (1.0) |
| New Hampshire Avenue and Peabody Street (Signalized) | B (14.0) | B (15.5) | B (14.4) | B (16.1) | B (15.0) | B (17.2) |
| New Hampshire Avenue and Quackenbos Street (Unsignalized) | A (0.1) | A (0.1) | A (0.1) | A (0.2) | A (0.5) | A (0.5) |
| New Hampshire Avenue and Rittenhouse Street and 3rd Street (Signalized) | B (13.2) | B (15.9) | B (13.9) | B (16.7) | B (17.5)* | B (16.3)* |

A (7.9) - Level of Service (Seconds of Delay per Vehicle)
*Results at the New Hampshire Avenue and Rittenhouse Street and $3^{\text {rd }}$ Street are based on optimizing signal timings in order to reduce delay along the eastbound and westbound approaches.

| Table 4 - Level of Service Summary at Site Driveways |  |  |
| :--- | :---: | :---: |
| INTERSECTION | 2009 Total Future Conditions |  |
|  | AM | PM |
| Sligo Mill Road and Site Driveway 1 (Unsignalized) | $\mathrm{A}(1.1)$ | $\mathrm{A}(0.6)$ |
| Sligo Mill Road and Site Driveway 2 (Unsignalized) | $\mathrm{A}(1.2)$ | $\mathrm{A}(0.4)$ |
| Sligo Mill Road and Site Driveway 3 (Unsignalized) | $\mathrm{A}(0.9)$ | $\mathrm{A}(0.2)$ |
| Peabody Street and Site Driveway 4 (Unsignalized) | $\mathrm{A}(0.2)$ | $\mathrm{A}(0.1)$ |
| Peabody Street and Site Driveway 5 (Unsignalized) | $\mathrm{A}(0.3)$ | $\mathrm{A}(0.2)$ |
| Rittenhouse Street and Site Driveway 6 (Unsignalized) | $\mathrm{A}(0.5)$ | $\mathrm{A}(0.8)$ |
| First Street and Site Driveway 7 (Unsignalized) | $\mathrm{A}(0.8)$ | $\mathrm{A}(0.6)$ |

A (1.7) - Level of Service (Seconds of Delay per Vehicle)

These results show that with existing and background traffic volumes, the study area intersections operate at a high level of service A and B.

The addition of the 6000 New Hampshire Avenue traffic will result in no change in the levels of service at the area intersections. The proposed development will result in marginal increases in vehicle delay. The increases in vehicle delay will range from 0.1 to 4.3 seconds per vehicle. While the traffic effects of the 6000 New Hampshire Avenue development will be measurable, they will not be perceptible.

These results show the benefits of the dispersal of site traffic resulting from the multiple access locations serving this site.

## Pedestrian Impact

There are existing sidewalks along all of the adjacent streets. The proposed 6000 New Hampshire Avenue development will provide sidewalk connections to these adjacent streets.

## CONCLUSIONS

As a result of this study, it is concluded that the area intersections will all operate at acceptable conditions with the 6000 New Hampshire Avenue residential development in place. The proposed development will have no effect on the intersection levels of service and they will continue to operate at levels of service A and B. The increases in vehicle delay will be marginal. The proposed development will have no perceptible effect on the area intersections.

The site access drives will operate at levels of service A. The multiple driveways will provide the opportunity for the dispersal of site traffic and the realignment of the existing driveway on New Hampshire Avenue with Quackenbros Street will consolidate two intersections into one. As a result, the site access drives and vehicle circulation system will operate in a safe and efficient manner.

The area is well served by transit including Metrorail and Metrobus. Pedestrian connections in the area will be enhanced by this development.

A total of 381 on-site parking spaces will be provided to serve the 199 residential units. This number of spaces satisfies the zoning requirements and the practical requirements of the development. As a result, there will be no spillover of parking into the surrounding community.

APPENDIX

## 2 Kimley-Hom and Associates, Inc. <br> Intersection Turning Movement Count Summary

Sligo Milj Road and Rittenhouse Street

| Date Counted: 26-May-05 | Jurisdiction: Washington, D.C. |
| :--- | :--- |
| Day of Week: Thursday | Counted by: RD, TJ |


| Start Time | Southbound on Siligo Miil |  |  |  |  | Westbound on Rittenhouse |  |  |  |  | Northbound on STIgo Mini |  |  |  |  | Eastbound |  |  |  |  | Voh. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | Peds | Total | Léft | IThiru | Rlight | Peds | Total | Left | Thru | Right | Peds | Total | Left | Thrü | Right | Peds | Total |  |
| 7:00 AM | 0 | 1 | 1 | 1 | 2 | 1 | 24 | 1 | 0 | 26 | 0 | 2 | 1 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 31 |
| 7:15 AM | 2 | 4 | 2 | 0 | 8 | 4 | 19 | 0 | 0 | 23 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 33 |
| 7:30 AM | 1 | 3 | 4 | 0 | 8 | 3 | 31 | 0 | 0 | 34 | 0 | 0 | 2 | 1 | 2 | 0 | 0 | 0 | 1 | 0 | 44 |
| 7:45 AM | 3 | 2 | 2 | 0 | 7 | 7 | 38 | 3 | 2. | 48 | 0 | 3 | 2 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 60 |
| 8:00 AM | 2 | 3 | 6 | 0 | 11 | 2 | 38 | 3 | 0 | 43 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 55 |
| 8:15 AM | 1 | 0 | 3 | 0 | 4 | 6 | ${ }^{68}$ | 0 | 0 | 32 | 0 | 3 | 4 | 1 | 7 | 0 | 0 | 0 | 1 | 0 | 43 |
| 8:30 AM | 0 | 5 | 2 | 0 | 7 | 2 | 22 | 0 | 0 | 24 | 0 | 2 | 4 | 1 | 6 | 0 | - | 0 | 1 | 0 | 37 |
| 8:45 AM | 1 | 3 | 0 | 0 | 4 | 4 | 15 | 2 | 0 | 21 | 0 | 1 | 1 | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 27 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | O | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| 9:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| $9: 30 \mathrm{AM}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |


| 7:00 AM | 6 | 10 | $\theta$ | 1 | 25 | 15 | 112 | 4 | 2 | 131 | 0 | 5 | 7 | 2 | 12 | 0 | 0 | 0 | 1 | 0 | 168 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7:15 AM | 8 | 12 | 14 | 0 | 34 | 16 | 126 | 6 | 2 | 148 | 1 | 3 | B | 1 | 10 | 0 | 0 | 0 | 2 | 0 | 192 |
| 7:30 AM | 7 | 8 | 15 | 0 | 30 | 18 | 133 | 6 | 2 | 157 | 1 | 6 | 8 | 2 | 15 | 0 | 0 | 0 | 3 | 0 | 202 |
| 7:45 AM | 6 | 10 | 13 | 0 | 29 | 17 | 124 | 6 | 2 | 147 | 1 | 8 | 10 | 2 | 19 | 0 | 0 | 0 | 3 | 0 | 195 |
| 8:00 AM | 4 | 11 | 11 | 0 | 23 | 14 | 101 | 5 | 0 | 120 | 1 | 6 | 9 | 2 | 16 | 0 | 0 | 0 | 4 | 0 | 162 |
| 8:15 AM | 2 | 8 | 5 | 0 | 15 | 12 | 83 | 2 | 0 | 77 | 0 | 6 | 9 | 2 | 15 | 0 | 0 | 0 | 3 | 0 | 107 |
| 8:30 AM | 1 | 8 | 2 | 0 | 11 | 6 | 37 | 2 | 0 | 45 | 0 | 3 | 5 | 1 | 8 | 0 | 0 | 0 | 2 | 0 | 64 |
| 8:45 AM | 1 | 3 | 0 | 0 | 4 | 4 | 15 | 2 | 0 | 21 | 0 | 1 | 1 | 0 | 2 | 0 | 0 | 0 | 4 | 0 | 27 |
| 9:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Paak Hour (Start Time)

| $7: 30$ AM | 7 | 8 | 15 | 0 | 30 | 18 | 133 | 6 | 2 | 157 | 1 | 6 | 8 | 2 | 15 | 0 | 0 | 0 | 3 | 0 | 202 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | Soutthbound on Sligo Miil |  |  |  |  | Westhound an Riltenhouse |  |  |  |  | Northbound on Silgo Minl |  |  |  |  | Eastbound |  |  |  |  | Voh. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | 1 Thn | Right | Peds | Total | Left | Thau | \|Right | Peds | Total | Left | 1 Thru | R Right | Peds | Total | Left | Thin | Right] | Peds | Total |  |
| 4:00 PM | 4 | 0 | 0 | 0 | 4 | 2 | 11 | 2 | 0 | 16 | 0 |  | 7 | 0 | $\theta$ | 0 | - | - | - | 0 | ${ }^{28}$ |
| 4:15 PM | 0 | 2 |  | 0 | 3 | 2 | 15 | 1 | 0 | 18 | 1 | 1 | 15 | 0 | 17 | 0 | 0 | 0 | 0 | 0 | ${ }^{3}$ |
| 4:30 PM | 5 | 1 | 1 | 0 | 7 | 1 | 11 | 0 | 0 | 12 | 1 | 3 | 9 | 0 | 43 | 0 | 0 | 0 | 0 | 0 | 32 |
| 4:45 PM | 2 | 1 | 1 | 0 | 4 | 1 | 6 | 3 | 0 | 10 | 3 | 0 | 12 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 28 |
| 5:00 PM | 6 | 3 | 1 | 0 | 10 | 0 | 9 | 2 |  | 11 |  | 4 | 13 | 0 | 19 | 0 | 0 | 0 | 0 | 0 | 40 |
| 5:15 PM | 0 | 0 | , | 0 | 3 | 1 | 8 | 1 | 0 | 10 | 2 | 1 | 20 | 0 | 23 | 0 | 0 | 0 | 0 | 0 | ${ }^{36}$ |
| 5:30 PM | ${ }^{6}$ | 3 | 0 | 0 | 9 | 1 | 3 | 4 | 0 | 8 | 1 | 4 | 43 | 0 | 18 | 0 | 0 | 0 | 0 | 0 | ${ }^{35}$ |
| 5:45 PM | 4 | 2 | 2 | 0 | 8 | 4 | 6 | 0 | 0 | 10 | 0 | 2 | 20 | 0 | 22 | 0 | 0 | 0 | 0 | 0 | 40 |
| 6:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| B:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |


| 4:00 PM | 17 | 4 | 3 | 0 | 18 | 6 | 43 | 6 | 0 | 55 | 5 | 6 | 43 | 0 | 54 | 0 | 0 | 0 | 0 | 0 | 127 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4:15 PM | 13 | 7 | 4 | 0 | 24 | 4 | 41 | 6 | 0 | 51 | 7 | 8 | 49 | 0 | 64 | 0 | 0 | 0 | 0 | 0 | 139 |
| 4:30 PM | 13 | 5 | 8 | 0 | 24 | 3 | 34 | B | 0 | 43 | 8 | 8 | 54 | 0 | 70 | 0 | 0 | 0 | 0 | 0 | 137 |
| 4:45 PM | 14 | 7 | 5 | 0 | 26 | 3 | 26 | 10 | 0 | 39 | 8 | $\theta$ | 58 | 0 | 75 | 0 | 0 | 0 | 0 | 0 | 140 |
| 5:00 PM | 16 | 8 | 6 | 0 | 30 | 8 | 28 | 7 | 0 | 33 | 5 | 11 | 68 | 0 | 82 | 0 | 0 | 0 | 0 | 0 | 451 |
| 5:15 PM | 10 | 5 | 5 | 0 | 20 | 8 | 17 | 5 | 0 | 28 | 3 | 7 | 53 | 0 | 63 | 0 | 0 | 0 | 0 | 0 | 111 |
| 5:30 PM | 10 | 5 | 2 | 0 | 17 | 8 | 9 | 4 | 0 | 18 | 1 | 6 | 33 | 0 | 40 | 0 | 0 | 0 | 0 | 0 | 75 |
| 5:45 PM | 4 | 2 | 2 | 0 | 8 | 4 | 6 | 0 | 0 | 10 | 0 | 2 | 20 | 0 | 22 | 0 | 0 | 0 | 0 | 0 | 40 |
| 6:00 FM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Peak Hour (Start Time) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:00 PM | 48 | 8 | 6 | 0 | 30 | 6 | 26 | 7 | 0 | 39 | 5 | 11 | 88 | 0 | 82 | 0 | 0 | 0 | 0 | 0 | 151 |





## New Hampshire Avenụa + Rittenhouse Street

Date Counted: May 24, 2005 (AM) and May 25, 2005 (PM)
Jurisdiction: Washington, D.C
Day of Week: Tuesday/Wednesday Weather: Rainy, warm/Sunny, warm

| Start Time | Southbound on New Hampshire |  |  |  |  | Westbound on Rittenhouse |  |  |  |  | Northbound on New Hampshire |  |  |  |  | Eastbound on Rittentouse |  |  |  |  | $\begin{aligned} & \text { Voh. } \\ & \text { rotal } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thiru | Right | Peds | Totă | Left | [Thiu | Right | Peds | ITatal | Left | Thru | Right | Peds | Total | Left | Thind | Right | Peds | Total |  |
| 7:00 AM | 0 | 336 | 1 | 2 | 340 | 21 | 15 | 4 | 0 | 40 | 1 | 78 | 7 | 3 | ${ }^{88}$ | 0 | 2 | 0 | 0 | 2 | 488 |
| 7:15 AM | 4 | 368 | 4 | 2 | 378 | 29 | 14 | 11 | 4 | 54 | 0 | 105 | 10 | 1 | 116 | 0 | 1 | 1 | 2 | 2 | 547 |
| 7:30 AM | 8 | 371 | 8 | 5 | 387 | 31 | 32 | 13 | 0 | 78 | 0 | 117 | 7 | 4 | 124 | 2 | 0 | 0 | 1 | 2 | 889 |
| 7:45 AM | 2 | 398 | 13 | 2 | 413 | 16 | 28 | 18 | 4 | 62 | 0 | 119 | 11 | 3 | 130 | 2 | 3 | 0 | 0 | 5 | 610 |
| 8:00 AM | 1 | 316 | 8 | 1 | 325 | 28 | 23 | 11 | 6 | 59 | 0 | 124 | 6 | 5 | 130 | 0 | 2 | 0 | 1 | 2 | 516 |
| 8:15 AM | 1 | 322 | 8 | 1 | 331 | 17 | 30 | 11 | 8 | 58 | 3 | 113 | 9 | 2 | 125 | 0 | 2 | 1 | 2 |  | 517 |
| 8:30 AM | 1 | 342 | 6 | 1 | 349 | 19 | 20 | 12 | 3 | 51 | 0 | 113 | 14 | 1 | 127 | 0 | 1 | 1 | 1 | 2 | 529 |
| 8:45 AM | 2 | 280 | 10 | 1 | 292 | 14 | 19 | 13 | 3 | 48 | 0 | 98 | 4 | 0 | 102 | 0 | 0 | 0 | 1 | 0 | 40 |
| 9:09 AM |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |


| 7:00 AM | 14 | 1473 | 20 | 11 | 1546 | 97 | 89 | 46 | 8 | 232 | 1 | 419 | 35 | 11 | 455 | 4 | 6 | 1 | 3 | 11 | 2214 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7:15 AM | 15 | 1463 | 33 | 10 | 1501 | 101 | 87 | 53 | 14 | 251 | 0 | 465 | 34 | 13 | 498 | 4 | 6 | 1 | 4 | 14 | 2282 |
| 7:30 AM | 12 | 1407 | 37 | 9 | 1458 | 89 | 113 | 53 | 18 | 255 | 3 | 473 | 33 | 14 | 509 | 4 | 7 | 1 | 4 | 12 | 2232 |
| 7:45 AM | 5 | 1378 | 35 | 5 | 1418 | 77 | 101 | 52 | 21 | 230 | 3 | 469 | 40 | 11 | 512 | 2 | 8 | 2 | 4 | 12 | 2172 |
| 8:00 AM | 5 | 1280 | 32 | 4 | 1297 | 75 | 92 | 47 | 20 | 214 | 3 | 448 | 33 | 8 | 484 | 0 | 5 | 2 | 5 | 7 | 2002 |
| 8:15 AM | 4 | 944 | 24 | 3 | 972 | 50 | 69 | 36 | 14 | 155 | 3 | 324 | 27 | 3 | 354 | 0 | 3 | 2 | 4 | 5 | 1488 |
| 8:30 AM | 3 | 622 | 18 | 2 | 649 | 33 | 39 | 23 | 6 | 97 | 0 | 211 | 18 | 1 | 229 | 0 | 1 | 1 | 2 | 2 | 969 |
| 8:45 AM | 2 | 280 | 10. | 1 | 292 | 14 | 19 | 13 | 3 | 48 | 0 | 88 | 4 | 0 | 102 | 0 | 0 | 0 | 1 | 0 | 440 |
| 9:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Peak Hour (Start Time)

| $7: 15$ A1 | 15 | 1453 | 33 | 10 | 1501 | 101 | 97 | 53 | 14 | 251 | 0 | 465 | 34 | 13 | 499 | 4 | 6 | 1 | 4 | 11 | 2282 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Start Time | Southbound on New Hampshire |  |  |  |  | Westhound on Rittenhouse |  |  |  |  | Northbound on New Hampshire |  |  |  |  | Eastbound on Rittenhouse |  |  |  |  | Veh. <br> Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | Peds | Total | Left | Thru | Right | Perds | Total | Left | Thru | Right | Peds | Total | Left | Thus | Right] | Pods | Total |  |
| 4:00 PM | 21 | 143 | 5 | 0 | 169 | 25 | 16 | 32 | 4 | 73 | 2 | 320 | 24 | 2 | 346 | 5 | 12 | 0 | 1 | 17 | 605 |
| 4:45 PM | 10 | 105 | 3 | 1 | 118 | 12 | 13 | 41 | 1 | 66 | 0 | 329 | 26 | 2 | 356 | 2 | 13 | 1 | 3 | 18 | 655 |
| 4:30 PM | 25 | 144 | 4 | 0 | 173 | 11 | 8 | 31 | 3 | 50 | 0 | 331 | 24 | 3 | 356 | 5 | 17 | 0 | 1 | 22 | 600 |
| 4:45 PM | 22 | 157 | 2 | 0 | 181 | 8 | 8 | 35 | 7 | 52 | 1 | 319 | 21 | 0 | 341 | 5 | 14 | 0 | 6 | 19 | 383 |
| 5:00 PM | 19 | 141 | 4 | 3 | 164 | 13 | 10 | 36 | 4 | 59 | 2 | 360 | 18 | 1 | 378 | 6 | 10 | 0 | 2 | 16 | 617 |
| 5:15 PM | 21 | 145 | 2 | 0 | 168 | 18 | 11 | 45 | 0 | 74 | 0 | 337 | 49 | 0 | 358 | 2 | 40 | 3 | 1 | 15 | 613 |
| 5:30 PM | 9 | 156 | 4 | 4 | 169 | 7 | 11 | 40 | 5 | 58 | 0 | 343 | 20 | 0 | 363 | 4 | 12 | 1 | 1 | 77 | 607 |
| 5:45' PM | 18 | 157 | 5 | 6 | 180 | 10 | 5 | 33 | 1 | 48 | 0 | 362 | 24 | 1 | 376 | 2 | $B$ | 3 | 2 | 13 | 617 |
| 6:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |


| 4:00 PM | 78 | 649 | 14 | 1 | 841 | 57 | 45 | 139 | 15 | 241 | 3 | 1299 | 95 | 7 | 1397 | 17 | 56 | 1 | 11 | 74 | 2353 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4:15 PM | 76 | 547 | 13 | 4 | 636 | 45 | 39 | 143 | 15 | 227 | 3 | 1339 | 87 | 6 | 1429 | 18 | 54 | 1 | 12 | 73 | 2085 |
| 4:30 PM | 87 | 587 | 12 | 3 | 686 | 51 | 37 | 147 | 14 | 235 | 3 | 1347 | 80 | 4 | 1430 | 18 | 51 | 3 | 10 | 72 | 2423 |
| 4:45 PM | 74 | 599 | 12 | 7 | 682 | 47 | 40 | 156 | 16 | 243 | 3 | 1359 | 76 | 1 | 1438 | 17 | 46 | 4 | 10 | 67 | 2430 |
| 5:00 PM | 67 | 659 | 15 | 13 | 681 | 48 | 37 | 154 | 10 | 239 | 2 | 7382 | 79 | 2 | 1473 | 14 | 40 | 7 | 6 | 61 | 2454 |
| 5:15 PM | 48 | 458 | 11 | 10 | 517 | 35 | 27 | 118 | 6 | 180 | 0 | 1032 | 63 | 1 | 1095 | 8 | 30 | $\boldsymbol{r}$ | 4 | 45 | 1837 |
| 5:30 PM | 27 | 313 | 9 | 10 | 349 | 17 | 16 | 73 | 6 | 106 | 0 | 696 | 44 | 1 | 739 | 6 | 20 | 4 | 3 | 30 | 1224 |
| 5:45 PM | 18 | 457 | 5 | 6 | 180 | 40 | 5 | 33 | 1 | 48 | 0 | 352 | 24 | 1 | 376 | 2 | 8 | 3 | 2 | 13 | 617 |
| 6:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Peak Hour (Start Time)





HCM Signalized Intersection Capacity Analysis
1: Peabody Street \& New Hampshire Avenue

|  |  |  |  |  |  |  |  | $\uparrow$ |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | 4 |  |  | 410 |  |  | 41 |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  |  | 4.0 |  |  | 4.0 |  |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  |  | 0.95 |  |  | 0.95 |  |
| Frpb, ped/bikes |  | 1.00 |  |  | 1.00 | 4 |  | 1.00 |  |  | 1.00 |  |
| Flpb, ped/bikes |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Frt |  | 0.98 |  |  | 1.00 | 4. |  | 1.00 |  |  | 1.00 |  |
| Flt Protected |  | 0.99 |  |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Satd. Flow (prot) |  | 1814 | 4 |  | 1854 |  |  | 3530 |  |  | 3522 |  |
| Flt Permitted |  | 0.92 |  |  | 0.97 |  |  | 0.90 |  |  | 1.00 |  |
| Satd. Flow (perm) |  | 1682 |  |  | 1810 | ¢ | d | 3177 |  |  | 3522 | 3 |
| Volume (vph) | 16 | 87 | 15 | 25 | 315 | 1 | 16 | 423 | 2 | 0 | 1142 | 31 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 16 | 90 | 15 | 26 | 325 | 1 | 16 | 436 | 2 | 0 | 1177 | 32 |
| Lane Group Flow (vph) | 0 | 121 | 0 | 0 | 352 | 0 | 0 | 454 | 0 | 0 | 1209 | 0 |
| Confl. Peds. (\#/hr) | 4 |  | 7 | 7 |  | 4 | 4 |  | 1 | 1 |  | 4 |
| Turn Type | Perm |  |  | Perm |  |  | Perm |  |  | Perm |  |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Actuated Green, G (s) |  | 25.0 |  |  | 25.0 |  |  | 65.0 |  |  | 65.0 |  |
| Effective Green, g (s) |  | 26.0 |  |  | 26.0 |  |  | 66.0 |  |  | 66.0 |  |
| Actuated g/C Ratio |  | 0.26 |  |  | 0.26 |  |  | 0.66 |  |  | 0.66 |  |
| Clearance Time (s) |  | 5.0 |  |  | 5.0 |  |  | 5.0 |  |  | 5.0 |  |
| Lane Grp Cap (vph) |  | 437 |  |  | 471 |  |  | 2097 |  |  | 2325 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  |  |  |  |  |  |  |  |  |  | c0.34 |  |
| v/s Ratio Perm |  | 0.07 |  |  | c0.19 |  |  | 0.14 |  |  |  |  |
| v/c Ratio |  | 0.28 |  |  | 0.75 |  |  | 0.22 |  |  | 0.52 |  |
| Uniform Delay, d1 |  | 29.5 |  |  | 34.0 |  |  | 6.7 |  |  | 8.8 |  |
| Progression Factor |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  | 0.61 |  |
| Incremental Delay, d2 |  | 1.6 |  |  | 10.4 |  |  | 0.2 |  |  | 0.7 |  |
| Delay (s) |  | 31.1 |  |  | 44.3 |  |  | 7.0 |  |  | 6.0 |  |
| Level of Service |  | C |  |  | D |  |  | A |  |  | A |  |
| Approach Delay (s) |  | 31.1 |  |  | 44.3 |  |  | 7.0 |  |  | 6.0 |  |
| Approach LOS |  | C |  |  | D |  |  | A |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control DelayHCM Volume to Capacity ratio |  |  | 14.0 | HCM Level of Service |  |  |  |  | B |  |  |  |
|  |  |  | 0.58 |  |  |  |  |  |  |  |  |  |
| HCM Volume to Capacity ratioCycle Length (s) |  |  | 100.0 | Sum of lost time (s) |  |  |  |  | 8.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 65.5\% | ICU Level of Service |  |  |  |  | B |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

HCM Signalized Intersection Capacity Analysis
2: Rittenhouse Street \& New Hampshire Avenue


HCM Signalized Intersection Capacity Analysis
2: Rittenhouse Street \& New Hampshire Avenue
07/07/2005


HCM Unsignalized Intersection Capacity Analysis
5: Peabody Street \& First Street


HCM Unsignalized Intersection Capacity Analysis
7: Peabody Street \&


HCM Unsignalized Intersection Capacity Analysis
8: Rittenhouse Street \& Sligo Mill Road

|  | $\rightarrow$ |  | 2 | $\cdots$ |  |  | $\dagger$ | $\nearrow$ | $\rightarrow$ | $\zeta$ |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  |  |  |  | ¢ |  |  | ¢ |  |  | ¢ |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Stop |  |  | Stop |  |
| Volume (veh/h) | 0 | 0 | 0 | 18 | 133 | 6 | 1 | 6 | 8 | 7 | 8 | 15 |
| Peak Hour Factor | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 |
| Hourly flow rate (veh/h) | 0 | 0 | 0 | 21 | 158 | 7 | 1 | 7 | 10 | 8 | 10 | 18 |
| Direction, Lane \# | WB 1 | NE 1 | SW 1 |  |  |  |  |  |  |  |  |  |
| Volume Total (vph) | 187 | 18 | 36 |  |  |  |  |  |  |  |  |  |
| Volume Left (vph) | 21 | 1 | 8 |  |  |  |  |  |  |  |  |  |
| Volume Right (vph) | 7 | 10 | 18 |  |  |  |  |  |  |  |  |  |
| Hadj (s) | 0.0 | -0.3 | -0.2 |  |  |  |  |  |  |  |  |  |
| Departure Headway (s) | 4.0 | 4.0 | 4.1 |  |  |  |  |  |  |  |  |  |
| Degree Utilization, x | 0.21 | 0.02 | 0.04 |  |  |  |  |  |  |  |  |  |
| Capacity (veh/h) | 876 | 844 | 844 |  |  |  |  |  |  |  |  |  |
| Control Delay (s) | 8.1 | 7.1 | 7.3 |  |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 8.1 | 7.1 | 7.3 |  |  |  |  |  |  |  |  |  |
| Approach LOS | A | A | A |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| DelayHCM Level of Service |  |  | 7.9 |  |  |  |  |  |  |  |  |  |
|  |  |  | A |  |  |  |  |  |  |  |  |  |
| HCM Level of ServiceIntersection Capacity Utilization |  |  | 24.6\% |  | ICU Level of Service |  |  |  | A |  |  |  |

HCM Unsignalized Intersection Capacity Analysis
10: Chillum Place \& Sligo Mill Road

|  | $\rightarrow$ | $\rightarrow$ |  |  | ¢ | $\checkmark$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | WBT | WBR | SWL | SWR |  |
| Lane Configurations |  | $\uparrow$ | $\dagger$ |  | Y |  |  |
| Sign Control |  | Free | Free |  | Stop |  |  |
| Grade |  | 0\% | 0\% |  | 0\% |  |  |
| Volume (veh/h) | 13 | 131 | 312 | 7 | 8 | 19 |  |
| Peak Hour Factor | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 |  |
| Hourly flow rate (veh/h) | 15 | 154 | 367 | 8 | 9 | 22 |  |
| Pedestrians |  |  |  |  | 18 |  |  |
| Lane Width (ft) |  |  |  |  | 12.0 |  |  |
| Walking Speed (fts) |  |  |  |  | 4.0 |  |  |
| Percent Blockage |  |  |  |  | 2 |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |
| Median type |  |  |  |  | None |  |  |
| Median storage veh) |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |
| VC, conflicting volume | 393 |  |  |  | 574 | 389 |  |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  |  |
| vCu , unblocked vol | 393 |  |  |  | 574 | 389 |  |
| tC , single (s) | 4.1 |  |  |  | 6.4 | 6.2 |  |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  |  |  |  |
| tF (s) | 2.2 |  |  |  | 3.5 | 3.3 |  |
| p0 queue free \% | 99 |  |  |  | 98 | 97 |  |
| cM capacity (veh/h) | 1148 |  |  |  | 467 | 649 |  |
| Direction, Lane \# | EB 1 | WB 1 | SW 1 |  |  |  |  |
| Volume Total | 169 | 375 | 32 |  |  |  |  |
| Volume Left | 15 | 0 | 9 |  |  |  |  |
| Volume Right | 0 | 8 | 22 |  |  |  |  |
| cSH | 1148 | 1700 | 582 |  |  |  |  |
| Volume to Capacity | 0.01 | 0.22 | 0.05 |  |  |  |  |
| Queue Length (ft) | 1 | 0 | 4 |  |  |  |  |
| Control Delay (s) | 0.8 | 0.0 | 11.5 |  |  |  |  |
| Lane LOS | A |  | B |  |  |  |  |
| Approach Delay (s) | 0.8 | 0.0 | 11.5 |  |  |  |  |
| Approach LOS |  |  | B |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.9 |  |  |  |  |
| Intersection Capacity Utilization |  |  | 29.9\% |  | CU Leve | of Service | A |

HCM Unsignalized Intersection Capacity Analysis
16: Quackenbos Street \& New Hampshire Avenue


HCM Signalized Intersection Capacity Analysis
1: Peabody Street \& New Hampshire Avenue

|  |  | $\rightarrow$ |  |  |  |  |  | $\uparrow$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | ¢ |  |  | 17 |  |  | $4 \%$ |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  |  | 4.0 |  |  | 4.0 |  |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  |  | 0.95 |  |  | 0.95 |  |
| Frpb, ped/bikes |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Flpb, ped/bikes |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Frt |  | 0.99 |  |  | 0.99 |  |  | 1.00 |  |  | 1.00 |  |
| Flt Protected |  | 0.99 |  |  | 0.99 |  |  | 1.00 |  |  | 1.00 |  |
| Satd. Flow (prot) |  | 1835 |  |  | 1826 |  |  | 3534 |  |  | 3525 | cede |
| Fit Permitted |  | 0.95 |  |  | 0.92 |  |  | 0.95 |  |  | 1.00 |  |
| Satd. Flow (perm) | - | 1748 |  |  | 1684 |  |  | 3366 |  |  | 3525 | 5 |
| Volume (vph) | 43 | 270 | 16 | 18 | 111 | 12 | 6 | 1206 | 8 | 0 | 639 | 14 |
| Peak-hour factor, PHF | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Adj. Flow (vph) | 46 | 287 | 17 | 19 | 118 | 13 | 6 | 1283 | 9 | 0 | 680 | 15 |
| Lane Group Flow (vph) | 0 | 350 | 0 | 0 | 150 | 0 | 0 | 1298 | 0 | 0 | 695 |  |
| Confl. Peds. (\#/hr) | 4 |  | 7 | 7 |  | 4 | 4 |  | 1 | 1 |  | 4 |
| Turn Type | Perm |  |  | Perm |  | * | Perm |  |  | Perm |  |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Actuated Green, G (s) |  | 25.0 |  |  | 25.0 |  |  | 65.0 |  |  | 65.0 |  |
| Effective Green, g (s) |  | 26.0 |  |  | 26.0 |  |  | 66.0 |  |  | 66.0 |  |
| Actuated g/C Ratio |  | 0.26 |  |  | 0.26 |  |  | 0.66 |  |  | 0.66 |  |
| Clearance Time (s) |  | 5.0 |  |  | 5.0 |  |  | 5.0 |  |  | 5.0 |  |
| Lane Grp Cap (vph) |  | 454 |  |  | 438 |  |  | 2222 |  |  | 2327 |  |
| v/s Ratio Prot |  |  |  |  |  |  |  |  |  |  | 0.20 |  |
| v/s Ratio Perm |  | c0.20 |  |  | 0.09 |  |  | c0.39 |  |  |  |  |
| v/c Ratio . |  | 0.77 |  |  | 0.34 |  |  | 0.58 |  |  | 0.30 |  |
| Uniform Delay, d1 |  | 34.2 |  |  | 30.1 |  |  | 9.4 |  |  | 7.2 |  |
| Progression Factor |  | 1.00 |  |  | 1.00 | 保 |  | 1.00 |  |  | 0.77 |  |
| Incremental Delay, d2 |  | 12.0 |  |  | 2.1 |  |  | 1.1 |  |  | 0.3 |  |
| Delay (s) |  | 46.2 |  |  | 32.2 | y-4krex |  | 10.5 |  |  | 5.9 |  |
| Level of Service |  | D |  |  | C |  |  | B |  |  | A |  |
| Approach Delay (s) |  | 46.2 |  |  | 32.2 | 4, 3.3 |  | 10.5 |  |  | 5.9 |  |
| Approach LOS |  | D |  |  | C |  |  | B |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 15.5 | HCM Level of Service |  |  |  |  | B |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.64 |  |  |  |  |  |  |  |  |  |
| Cycle Length (s) |  |  | 100.0 | Sum of lost time (s) |  |  |  |  | 8.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 79.8\% | ICU Level of Service |  |  |  |  | C |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

HCM Signalized Intersection Capacity Analysis
2: Rittenhouse Street \& New Hampshire Avenue
07/07/2005


HCM Signalized Intersection Capacity Analysis
2: Rittenhouse Street \& New Hampshire Avenue
07/07/2005

|  | $\ldots$ |  |  |  | 4 | $\stackrel{+}{ }$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | SBL | SBT | SBR | NWL | NWR | NWR2 |  |  |  |
| Lane Configurations | \% | * |  | \% | - | 7 |  |  | deytar |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |  |  |
| Total Lost time (s) | 4.0 | 4.0 |  | 4.0 | - | 4.0 |  |  |  |
| Lane Util. Factor | 1.00 | 0.95 |  | 1.00 |  | 0.95 |  |  |  |
| Frpb, ped/bikes | 1.00 | 1.00 |  | 0.96 |  | 0.96 |  |  |  |
| Flpb, ped/bikes | 1.00 | 1.00 |  | 1.00 |  | 1.00 |  |  |  |
| Frt | 1.00 | 1.00 |  | 0.86 |  | 0.85 |  |  |  |
| Flt Protected | 0.95 | 1.00 |  | 1.00 |  | 1.00 |  |  |  |
| Satd. Flow (prot) | 1770 | 3520 |  | 1531 | ${ }^{3+m}$ | 1442 |  | 3 |  |
| Fit Permitted | 0.95 | 1.00 |  | 1.00 |  | 1.00 |  |  |  |
| Satd. Flow (perm) | 1770 | 3520 |  | 1531 | 103023 | 1442 |  |  | - |
| Volume (vph) | 58 | 599 | 18 | 4 | 100 | 15 |  |  |  |
| Peak-hour factor, PHF | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 |  |  | - |
| Adj. Flow (vph) | 59 | 605 | 18 | 4 | 101 | 15 |  |  |  |
| Lane Group Flow (vph) | 68 | 623 | 0 | 105 | 0 | - 15 |  |  |  |
| Confl. Peds. (\#/hr) | 14 |  | 4 | 4 | 10 | 14 |  |  |  |
| Turn Type | Prot |  |  |  | a -9 | ustom |  |  | - 2 cely |
| Protected Phases | 14 |  |  |  |  |  |  |  |  |
| Permitted Phases |  | 614 |  | 10 | \% | 2 |  |  |  |
| Actuated Green, G (s) | 10.0 | 75.0 |  | 10.0 |  | 60.0 |  |  |  |
| Effective Green, g (s) | 11.0 | 76.0 |  | 11.0 | Y4 | 61.0 | \% |  |  |
| Actuated g/C Ratio | 0.11 | 0.76 |  | 0.11 |  | 0.61 |  |  |  |
| Clearance Time (s) | 5.0 |  |  | 5.0 | -ma | 5.0 | 8 |  |  |
| Lane Grp Cap (vph) | 195 | 2675 |  | 168 |  | 880 |  |  |  |
| v/s Ratio Prot | 0.04 |  |  |  |  |  |  |  |  |
| v/s Ratio Perm |  | 0.18 |  | c0.07 |  | 0.01 |  |  |  |
| V/c Ratio | 0.35 | 0.23 |  | 0.62 | $*$ | 0.02 |  |  |  |
| Uniform Delay, d1 | 41.2 | 3.5 |  | 42.5 |  | 7.7 |  |  |  |
| Progression Factor | 1.00 | 1.00 |  | 1.00 |  | 1.00 |  |  |  |
| Incremental Delay, d2 | 4.9 | 0.2 |  | 16.3 |  | 0.0 |  |  |  |
| Delay (s) | 46.0 | 3.7 |  | 58.8 |  | 7.7 |  |  |  |
| Level of Service | D | A |  | E |  | A |  |  |  |
| Approach Delay (s) |  | 7.9 |  | 52.4 |  |  |  |  | 6 |
| Approach LOS |  | A |  | D |  | (1) |  | $=$ | - |
| Intersection Summary |  |  |  |  |  |  |  |  |  |



HCM Unsignalized Intersection Capacity Analysis

## 7: Peabody Street \&

|  | 5 |  |  |  | $\rightarrow$ | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | WBT | WBR | SEL | SER |  |
| Lane Configurations |  | $\uparrow$ | $\dagger$ |  | \% |  |  |
| Sign Control |  | Free | Free |  | Stop |  |  |
| Grade |  | 0\% | 0\% |  | 0\% |  |  |
| Volume (veh/h) | 2 | 5 | 6 | 355 | 131 | 5 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |  |
| Hourly flow rate (veh/h) | 2 | 5 | 7 | 386 | 142 | 5 |  |
| Pedestrians |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |
| Walking Speed (ft/s) |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |
| Median type |  |  |  |  | None |  |  |
| Median storage veh) |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  | 569 |  |  |  |  |
| pX , platoon unblocked |  |  |  |  |  |  |  |
| VC, conflicting volume | 392 |  |  |  | 209 | 199 |  |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |
| VC 2 , stage 2 conf vol |  |  |  |  |  |  |  |
| vCu, unblocked vol | 392 |  |  |  | 209 | 199 |  |
| tC, single (s) | 4.1 |  |  |  | 6.4 | 6.2 |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |
| tF (s) | 2.2 |  |  |  | 3.5 | 3.3 |  |
| p0 queue free \% | 100 |  |  |  | 82 | 99 |  |
| CM capacity (veh/h) | 1166 |  |  |  | 778 | 842 |  |
| Direction, Lane \# | EB 1 | WB 1 | SE 1 |  |  |  |  |
| Volume Total | 8 | 392 | 148 |  |  |  |  |
| Volume Left | 2 | 0 | 142 |  |  |  |  |
| Volume Right | 0 | 386 | 5 |  |  |  |  |
| cSH | 1166 | 1700 | 780 |  |  |  |  |
| Volume to Capacity | 0.00 | 0.23 | 0.19 |  |  |  |  |
| Queue Length (ft) | 0 | 0 | 17 |  |  |  |  |
| Control Delay (s) | 2.3 | 0.0 | 10.7 |  |  |  |  |
| Lane LOS | A |  | B |  |  |  |  |
| Approach Delay (s) | 2.3 | 0.0 | 10.7 |  |  |  |  |
| Approach LOS |  |  | B |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 2.9 |  |  |  |  |
| Intersection Capacity Utilization |  |  | 39.1\% |  | ICU Leve | of Service | A |

HCM Unsignalized Intersection Capacity Analysis
8: Rittenhouse Street \& Sligo Mill Road
07/07/2005

|  | $\rightarrow$ |  | 7 | - |  | $\checkmark$ | ) | $\ngtr$ | $\rho$ | $\zeta$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  |  |  |  | $\dagger$ |  |  | ¢ |  |  | ¢ |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Stop |  |  | Stop |  |
| Volume (veh/h) | 0 | 0 | 0 | 6 | 26 | 7 | 5 | 11 | 66 | 16 | 8 | 6 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Hourly flow rate (veh/h) | 0 | 0 | 0 | 6 | 28 | 7 | 5 | 12 | 70 | 17 | 9 | 6 |
| Direction, Lane \# | WB 1 | NE 1 | SW 1 |  |  |  |  |  |  |  |  |  |
| Volume Total (vph) | 41 | 87 | 32 |  |  |  |  |  |  |  |  |  |
| Volume Left (vph) | 6 | 5 | 17 |  |  |  |  |  |  |  |  |  |
| Volume Right (vph) | 7 | 70 | 6 |  |  |  |  |  |  |  |  |  |
| Hadj (s) | 0.0 | -0.4 | 0.0 |  |  |  |  |  |  |  |  |  |
| Departure Headway (s) | 4.1 | 3.6 | 4.1 |  |  |  |  |  |  |  |  |  |
| Degree Utilization, x | 0.05 | 0.09 | 0.04 |  |  |  |  |  |  |  |  |  |
| Capacity (veh/h) | 855 | 982 | 867 |  |  |  |  |  |  |  |  |  |
| Control Delay (s) | 7.3 | 6.9 | 7.2 |  |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 7.3 | 6.9 | 7.2 |  |  |  |  |  |  |  |  | (3) |
| Approach LOS | A | A | A |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Delay |  |  | 7.1 |  |  |  |  |  |  |  |  |  |
|  |  |  | A |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 16.7\% |  | ICU Level of Service |  |  |  | A |  |  |  |

HCM Unsignalized Intersection Capacity Analysis
10: Chillum Place \& Sligo Mill Road



HCM Signalized Intersection Capacity Analysis
1: Peabody Street \& New Hampshire Avenue


HCM Signalized Intersection Capacity Analysis
2: Rittenhouse Street \& New Hampshire Avenue

|  |  |  |  |  |  |  |  | 4 | 4 | $p$ |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | EBR2 | WBL2 | WBL | WBT | WBR | NBT | NBR | SBL2 | SBL |
| Lane Configurations |  | ¢ |  |  |  |  | ¢ |  | fit |  |  | ${ }^{5}$ |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 |  |  |  |  | 4.0 |  | 4.0 |  |  | 4.0 |
| Lane Util. Factor |  | 1.00 |  |  |  |  | 1.00 |  | 0.95 |  |  | 1.00 |
| Frpb, ped/bikes |  | 0.98 |  |  |  |  | 1.00 |  | 1.00 |  |  | 1.00 |
| Flpb, ped/bikes |  | 1.00 |  |  |  |  | 0.97 |  | 1.00 |  |  | 1.00 |
| Frt |  | 0.96 |  |  |  |  | 1.00 |  | 0.99 |  |  | 1.00 |
| Flt Protected |  | 0.98 |  |  |  |  | 0.97 |  | 1.00 |  |  | 0.95 |
| Satd. Flow (prot) |  | 1724 |  |  |  |  | 1759 |  | 3493 |  |  | 1770 |
| Flt Permitted |  | 0.92 |  |  |  |  | 0.83 |  | 1.00 |  |  | 0.95 |
| Satd. Flow (perm) |  | 1608 |  |  |  |  | 1492 |  | 3493 |  |  | 1770 |
| Volume (vph) | 4 | 4 | 2 | 1 | 16 | 89 | 89 | 1 | 484 | 35 | 3 | 12 |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Adj. Flow (vph) | 4 | 4 | 2 | 1 | 17 | 96 | 96 | 1 | 520 | 38 | 3 | 13 |
| Lane Group Flow (vph) | 0 | 11 | 0 | 0 | 0 | 0 | 210 | 0 | 558 | 0 | 0 | 16 |
| Confl. Peds. (\#/hr) | 10 |  | 13 | 13 | 13 | 13 |  | 10 |  | 14 | 14 | 14 |
| Turn Type | Perm |  |  |  | Perm | Perm |  |  |  |  | Prot | Prot |
| Protected Phases |  | 4 |  |  |  |  | 8 |  |  |  | 14 | 14 |
| Permitted Phases | 4 |  |  |  | 8 | 8 |  |  | 2 |  |  |  |
| Actuated Green, G (s) |  | 15.0 |  |  |  |  | 15.0 |  | 60.0 |  |  | 10.0 |
| Effective Green, g (s) |  | 16.0 |  |  |  |  | 16.0 |  | 61.0 |  |  | 11.0 |
| Actuated g/C Ratio |  | 0.16 |  |  |  |  | 0.16 |  | 0.61 |  |  | 0.11 |
| Clearance Time (s) |  | 5.0 |  |  |  |  | 5.0 |  | 5.0 |  |  | 5.0 |
| Lane Grp Cap (vph) |  | 257 |  |  |  |  | 239 |  | 2131 |  |  | 195 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  |  |  |  |  |  |  |  |  |  |  | 0.01 |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm |  | 0.01 |  |  |  |  | c0.14 |  | 0.16 |  |  |  |
| $\mathrm{v} / \mathrm{c}$ Ratio |  | 0.04 |  |  |  |  | 0.88 |  | 0.26 |  |  | 0.08 |
| Uniform Delay, d1 |  | 35.5 |  |  |  |  | 41.1 |  | 9.1 |  |  | 40.0 |
| Progression Factor |  | 1.00 |  |  |  |  | 1.00 |  | 0.86 |  |  | 1.00 |
| Incremental Delay, d2 |  | 0.3 |  |  |  |  | 33.7 |  | 0.3 |  |  | 0.8 |
| Delay (s) |  | 35.8 |  |  |  |  | 74.8 |  | 8.0 |  |  | 40.8 |
| Level of Service |  | D |  |  |  |  | E |  | A |  |  | D |
| Approach Delay (s) |  | 35.8 |  |  |  |  | 74.8 |  | 8.0 |  |  |  |
| Approach LOS |  | D |  |  |  |  | E |  | A |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 13.9 |  | HCM Lev | el of S | ervice |  | B |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.67 |  |  |  |  |  |  |  |  |  |
| Cycle Length (s) |  |  | 100.0 |  | Sum of los | st time | (s) |  | 8.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 87.5\% |  | ICU Leve | of Se | vice |  | D |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

HCM Signalized Intersection Capacity Analysis
2: Rittenhouse Street \& New Hampshire Avenue
07/07/2005


HCM Unsignalized Intersection Capacity Analysis
5: Peabody Street \& First Street
07/07/2005


HCM Unsignalized Intersection Capacity Analysis
7: Peabody Street \&

|  |  |  |  |  | $\rightarrow$ | 4 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | WBT | WBR | SEL | SER |  |  |
| Lane Configurations |  | ${ }_{4}$ | F |  | M |  |  |  |
| Sign Control |  | Free | Free |  | Stop |  |  |  |
| Grade |  | 0\% | 0\% |  | 0\% |  |  |  |
| Volume ( $\mathrm{veh} / \mathrm{h}$ ) | 2 | 5 | 6 | 355 | 131 | 5 |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |  |  |
| Hourly flow rate (veh/h) | 2 | 5 | 7 | 386 | 142 | 5 |  |  |
| Pedestrians |  |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |  |
| Walking Speed (ft/s) |  |  |  |  |  | Y |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  | None |  |  |  |
| Median storage veh) |  |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  | 569 |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  | 4 |  |  | * |
| VC , conflicting volume | 392 |  |  |  | 209 | 199 |  |  |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  | TET |
| VC2, stage 2 conf vol |  |  |  |  |  |  |  |  |
| vCu , unblocked vol | 392 |  |  |  | 209 | 199 |  |  |
| tC, single (s) | 4.1 |  |  |  | 6.4 | 6.2 |  |  |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  |  |  |  |  |
| tF (s) | 2.2 |  |  |  | 3.5 | 3.3 |  |  |
| p0 queue free \% | 100 |  |  |  | 82 | 99 |  |  |
| cM capacity (veh/h) | 1166 |  |  |  | 778 | 842 |  |  |
| Direction, Lane \# | EB 1 | WB 1 | SE 1 |  |  |  |  |  |
| Volume Total | 8 | 392 | 148 |  |  |  |  |  |
| Volume Left | 2 | 0 | 142 |  |  |  |  | : |
| Volume Right | 0 | 386 | 5 |  |  |  |  |  |
| cSH | 1166 | 1700 | 780 |  |  |  |  |  |
| Volume to Capacity | 0.00 | 0.23 | 0.19 |  |  |  |  |  |
| Queue Length ( ft ) | 0 | 0 | 17. |  |  |  |  |  |
| Control Delay (s) | 2.3 | 0.0 | 10.7 |  |  |  |  |  |
| Lane LOS | A |  | B |  |  |  |  |  |
| Approach Delay (s) | 2.3 | 0.0 | 10.7 |  |  |  |  |  |
| Approach LOS |  |  | B |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 2.9 |  | ICU Level of Service |  | A |  |
| Intersection Capacity Util | lization |  | 39.1\% |  |  |  |  |  |

HCM Unsignalized Intersection Capacity Analysis
8: Rittenhouse Street \& Sligo Mill Road

|  | $\rightarrow$ | $\rightarrow$ | 2 | $\sim$ |  | 1 |  | $\not$ | $\rho$ | $\checkmark$ |  | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  |  |  |  | ${ }_{\text {¢ }}$ | + |  | ¢ |  |  | 4 |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Stop |  |  | Stop |  |
| Volume (veh/h) | 0 | 0 | 0 | 19 | 138 | 6 | 1 | 6 | 8 | 7 | 8 | 16 |
| Peak Hour Factor | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 |
| Hourly flow rate (veh/h) | 0 | 0 | 0 | 23 | 164 | 7 | 1 | 7 | 10 | 8 | 10 | 19 |
| Direction, Lane \# | WB 1 | NE 1 | SW 1 |  |  |  |  |  |  |  |  |  |
| Volume Total (vph) | 194 | 18 | 37 |  |  |  |  |  |  |  |  |  |
| Volume Left (vph) | 23 | 1 | 8 |  |  |  |  |  |  |  |  |  |
| Volume Right (vph) | 7 | 10 | 19 |  |  |  |  |  |  |  |  |  |
| Hadj (s) | 0.0 | -0.3 | -0.2 |  |  |  |  |  |  |  |  |  |
| Departure Headway (s) | 4.0 | 4.1 | 4.1 |  |  |  |  |  |  |  |  |  |
| Degree Utilization, x | 0.22 | 0.02 | 0.04 |  |  |  |  |  |  |  |  |  |
| Capacity (veh/h) | 875 | 840 | 842 |  |  |  |  |  |  |  |  |  |
| Control Delay (s) | 8.2 | 7.1 | 7.3 |  |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 8.2 | 7.1 | 7.3 |  |  |  |  |  |  |  |  |  |
| Approach LOS | A | A | A |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| DelayHCM Level of Service |  |  | 8.0 |  |  |  |  |  |  |  |  |  |
|  |  |  | A |  |  |  |  |  |  |  |  |  |
| HCM Level of ServiceIntersection Capacity Utilization |  |  | 25.5\% |  | ICU Level of Service |  |  |  | A |  |  |  |

HCM Unsignalized Intersection Capacity Analysis
10: Chillum Place \& Sligo Mill Road 07/07/2005


HCM Unsignalized Intersection Capacity Analysis
16: Quackenbos Street \& New. Hampshire Avenue


HCM Signalized Intersection Capacity Analysis
1: Peabody Street \& New Hampshire Avenue


HCM Signalized Intersection Capacity Analysis
2: Rittenhouse Street \& New Hampshire Avenue

|  |  |  |  |  | 6 | 1 |  |  | 4 | 4 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | EBR2 | WBL2 | WBL | WBT | WBR | NBL | NBT | NBR | SBL2 |
| Lane Configurations |  | 4 |  |  | ग- | * | ¢ |  | \% | AT |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 |  |  |  |  | 4.0 |  |  | 4.0 |  |  |
| Lane Util. Factor |  | 1.00 |  |  |  |  | 1.00 |  |  | 0.95 |  |  |
| Frpb, ped/bikes |  | 0.98 |  |  | - |  | 0.99 |  |  | 1.00 |  |  |
| Flpb, ped/bikes |  | 1.00 |  |  |  |  | 0.98 |  |  | 1.00 |  |  |
| Frt |  | 0.96 |  |  |  |  | 0.96 |  |  | 0.99 |  |  |
| Fit Protected |  | 0.99 |  |  |  |  | 0.98 |  |  | 1.00 |  |  |
| Satd. Flow (prot) |  | 1728 |  |  | \% |  | 1694 |  |  | 3503 |  |  |
| Flt Permitted |  | 0.93 |  |  |  |  | 0.88 |  |  | 0.86 |  |  |
| Satd. Flow. (perm) |  | 1629 |  |  | itacis | 4 | 1515 |  |  | 3021 |  | 2 |
| Volume (vph) | 15 | 27 | 10 | 7 | 3 | 47 | 34 | 41 | 2 | 1449 | 82 | 9 |
| Peak-hour factor, PHF | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 | 0.99 |
| Adj. Flow (vph) | 15 | 27 | 10 | 7 | 3 | 47 | 34 | 41 | 2 | 1464 | 83 | 9 |
| Lane Group Flow (vph) | 0 | 59 | 0 | 0 | 0 | 0 | 125 | 0 | 0 | 1549 |  | 4 |
| Confl. Peds. (\#/hr) | 10 |  | 13 | 13 | 13 | 13 |  | 10 | 4 |  | 14 | 14 |
| Turn Type | Perm |  |  |  | Perm | Perm |  |  | ustom |  |  | Prot |
| Protected Phases |  | 4 |  |  |  |  | 8 |  |  |  |  | 14 |
| Permitted Phases | 4 |  |  |  | 8 | 8 |  |  | 2 | 2 |  | \% |
| Actuated Green, G (s) |  | 15.0 |  |  |  |  | 15.0 |  |  | 60.0 |  |  |
| Effective Green, g (s) |  | 16.0 |  |  |  | \% | 16.0 |  | \$ | 61.0 |  | \%re |
| Actuated g/C Ratio |  | 0.16 |  |  |  |  | 0.16 |  |  | 0.61 |  |  |
| Clearance Time (s) |  | 5.0 |  |  |  | \% | 5.0 |  |  | 5.0 |  |  |
| Lane Grp Cap (vph) |  | 261 |  |  |  |  | 242 |  |  | 1843 |  |  |
| v/s Ratio Prot |  |  |  |  |  | \% |  |  |  |  |  |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm |  | 0.04 |  |  |  |  | c0.08 |  |  | c0.51 |  |  |
| v/c Ratio |  | 0.23 |  | - |  |  | 0.52 |  |  | 0.84 |  |  |
| Uniform Delay, d1 |  | 36.6 |  |  |  |  | 38.5 |  |  | 15.6 |  |  |
| Progression Factor |  | 1.00 | 2 |  |  |  | 1.00 |  |  | 0.66 |  |  |
| Incremental Delay, d2 |  | 2.0 |  |  |  |  | 7.7 |  |  | 4.2 |  |  |
| Delay (s) |  | 38.6 |  |  |  |  | 46.1 |  |  | 14.5 |  |  |
| Level of Service |  | D |  |  |  |  | D |  |  | B |  |  |
| Approach Delay (s) |  | 38.6 |  |  |  |  | 46.1 |  |  | 14.5 |  |  |
| Approach LOS |  | D |  |  |  |  | D |  |  | B |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 16.7 |  | HCM Le | el of S | ervice |  | B |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.76 |  |  |  |  |  |  |  |  |  |
| Cycle Length (s) |  |  | 100.0 |  | Sum of | st time | (s) |  | 12.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 2.1\% |  | ICU Lev | of Se | vice |  | F |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

HCM Signalized Intersection Capacity Analysis
2: Rittenhouse Street \& New Hampshire Avenue

|  | $\downarrow$ | $\downarrow$ |  | 4 | $\pm$ | $\stackrel{ }{ }+$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | SBL | SBT | SBR | NWL | NWR | WR2 |
| Lane Configurations | ${ }_{0}$ | 个t |  | ${ }_{0}$ |  | 7 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 |  | 4.0 |  | 4.0 |
| Lane Util. Factor | 1.00 | 0.95 |  | 1.00 |  | 0.95 |
| Frpb, ped/bikes | 1.00 | 1.00 |  | 0.96 |  | 0.96 |
| Flpb, ped/bikes | 1.00 | 1.00 |  | 1.00 |  | 1.00 |
| Frt | 1.00 | 1.00 |  | 0.86 |  | 0.85 |
| Fit Protected | 0.95 | 1.00 |  | 1.00 |  | 1.00 |
| Satd. Flow (prot) | 1770 | 3520 |  | 1530 |  | 1442 |
| Flt Permitted | 0.95 | 1.00 |  | 1.00 |  | 1.00 |
| Satd. Flow (perm) | 1770 | 3520 |  | 1530 |  | 1442 |
| Volume (vph) | 60 | 623 | 19 | 4 | 104 | 16 |
| Peak-hour factor, PHF | 0.99 | 0.99 | 0.99 | 0.90 | 0.99 | 0.99 |
| Adj. Flow (vph) | 61 | 629 | 19 | 4 | 105 | 16 |
| Lane Group Flow (vph) | 70 | 648 | 0 | 109 | 0 | 16 |
| Confl. Peds. (\#/hr) | 14 |  | 4 | 4 | 10 | 14 |
| Turn Type | Prot |  |  |  |  | stom |
| Protected Phases | 14 |  |  |  |  |  |
| Permitted Phases |  | 614 |  | 10 |  | 2 |
| Actuated Green, G (s) | 10.0 | 75.0 |  | 10.0 |  | 60.0 |
| Effective Green, g (s) | 11.0 | 76.0 |  | 11.0 |  | 61.0 |
| Actuated g/C Ratio | 0.11 | 0.76 |  | 0.11 |  | 0.61 |
| Clearance Time (s) | 5.0 |  |  | 5.0 |  | 5.0 |
| Lane Grp Cap (vph) | 195 | 2675 |  | 168 |  | 880 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot | 0.04 |  |  |  |  |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm |  | 0.18 |  | c0.07 |  | 0.01 |
| v/c Ratio | 0.36 | 0.24 |  | 0.65 |  | 0.02 |
| Uniform Delay, d1 | 41.2 | 3.5 |  | 42.6 |  | 7.7 |
| Progression Factor | 1.00 | 1.00 |  | 1.00 |  | 1.00 |
| Incremental Delay, d2 | 5.1 | 0.2 |  | 17.8 |  | 0.0 |
| Delay (s) | 46.3 | 3.7 |  | 60.4 |  | 7.7 |
| Level of Service | D | A |  | E |  | A |
| Approach Delay (s) |  | 7.9 |  | 53.7 |  |  |
| Approach LOS |  | A |  | D |  |  |
| Intersection Summary |  |  |  |  |  |  |



HCM Unsignnalized Intersection Capacity Analysis
7: Peabody Street \&

|  | 3 |  |  |  | $\rightarrow$ | 4 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | WBT | WBR | SEL | SER |  |  |
| Lane Configurations |  | $\uparrow$ | A |  | ${ }^{1}$ |  |  |  |
| Sign Control |  | Free | Free |  | Stop |  |  |  |
| Grade |  | 0\% | 0\% |  | 0\% |  |  | 7p+4x |
| Volume ( $\mathrm{veh} / \mathrm{h}$ ) | 2 | 5 | 6 | 355 | 131 | 5 |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |  | S |
| Hourly flow rate (veh/h) | , | 5 | 7 | 386 | 142 | 5 |  |  |
| Pedestrians |  |  |  |  |  |  |  | $8{ }^{2}$ |
| Lane Width (ft) |  |  |  |  |  |  |  |  |
| Walking Speed (ft/s) |  |  |  | 3 |  |  |  | - ${ }^{\text {cas }}$ |
| Percent Blockage |  |  |  |  |  |  |  |  |
| Rightturn flare (veh) |  |  |  |  |  |  |  | 4.38 |
| Median type |  |  |  |  | None |  |  |  |
| Median storage veh) |  |  |  |  |  |  |  | , |
| Upstream signal (ft) |  |  | 569 |  |  |  |  |  |
| pX , platoon unblocked |  |  |  |  | 崖 |  |  | Wry |
| VC, conflicting volume | 392 |  |  |  | 209 | 199 |  |  |
| $\mathrm{vC1}$; stage 1 conf vol |  |  |  |  |  |  |  | \% |
| VC2, stage 2 conf vol |  |  |  |  |  |  |  |  |
| vCu , unblocked vol | 392 |  |  | 2 1 | 209 | 199 |  |  |
| tC, single (s) | 4.1 |  |  |  | 6.4 | 6.2 |  |  |
| tC, 2 stage (s) |  |  | \% |  |  | 䍂 8 |  |  |
| tF (s) | 2.2 |  |  |  | 3.5 | 3.3 |  |  |
| po queue free \% | 100 |  |  |  | 82 | 99 : |  | - |
| CM capacity (veh/h) | 1166 |  |  |  | 778 | 842 |  |  |
| Direction, Lane \# | EB 1 | WB 1 | SE 1 |  |  |  |  |  |
| Volume Total | 8 | 392 | 148 |  |  |  |  |  |
| Volume Left | 2 | 0 | 142 |  |  |  |  |  |
| Volume Right | 0 | 386 | 5 |  |  |  |  |  |
| cSH | 1166 | 1700 | 780 |  |  |  |  | 5 \% |
| Volume to Capacity | 0.00 | 0.23 | 0.19 |  |  |  |  |  |
| Queue Length ( ft ) | 0 | 0 | 17 |  |  |  |  |  |
| Control Delay (s) | 2.3 | 0.0 | 10.7 |  |  |  |  |  |
| Lane LOS | A |  | B |  |  | \% |  |  |
| Approach Delay (s) | 2.3 | 0.0 | 10.7 |  |  |  |  |  |
| Approach LOS |  |  | B |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 2.9 Emper |  |  |  | A |  |
|  |  |  | 39.1\% | ICU Level of Service |  |  |  |  |

HCM Unsignalized Intersection Capacity Analysis
8: Rittenhouse Street \& Sligo Mill Road

|  | $\rightarrow$ | $\rightarrow$ | 2 | $\cdots$ | $\leftarrow$ | 1 | 3 | 7 | $p$ | 4 | $k$ | / |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  |  |  |  | ¢ |  |  | ¢ |  |  | 4 |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Stop |  |  | Stop |  |
| Volume (veh/h) | 0 | 0 | 0 | 6 | 27 | 7 | 5 | 11 | 69 | 17 | 8 | 6 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Hourly flow rate (veh/h) | 0 | 0 | 0 | 6 | 29 | 7 | 5 | 12 | 73 | 18 | 9 | 6 |

Direction, Lane \# WB 1 NE 1 SW

| Volume Total (vph) | 43 | 90 | 33 |
| :--- | :--- | :--- | :--- |


| Volume Left (vph) | 6 | 5 | 18 |
| :--- | :--- | ---: | ---: |


| Volume Right (vph) | 7 | 73 | 6 |
| :--- | ---: | ---: | ---: |
| Hadj (s) | 0.0 | -0.4 | 0.0 |


| Departure Headway (s) | 4.1 | 3.6 | 4.1 |
| :--- | ---: | ---: | ---: |
| Degree Utilization, x | 0.05 | 0.09 | 0.04 |
| Capacity (veh/h) | 853 | 982 | 865 |
| Control Delay (s) | 7.3 | 6.9 | 7.2 |
| Approach Delay (s) | 7.3 | 6.9 | 7.2 |

Approach LOS A A A

Intersection Summary
Delay
HCM Level of Service 7.1
Intersection Capacity Utilization $\quad 17.0 \% \quad$ ICU Level of Service A

HCM Unsignalized Intersection Capacity Analysis
10: Chillum Place \& Sligo Mill Road

|  | $\rightarrow$ | $\rightarrow$ |  | 1 | 4 | 4 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | WBT | WBR | SWL | SWR |  |
| Lane Configurations |  | $\uparrow$ | A |  | ${ }^{*}$ |  |  |
| Sign Control |  | Free | Free |  | Stop |  |  |
| Grade |  | 0\% | 0\% |  | 0\% |  |  |
| Volume (veh/h) | 65 | 281 | 149 | 8 | 10 | 5 |  |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |  |
| Hourly flow rate (veh/h) | 68 | 293 | 155 | 8 | 10 | 5 |  |
| Pedestrians |  |  |  |  | 18 |  |  |
| Lane Width (ft) |  |  |  |  | 12.0 |  |  |
| Walking Speed (ft/s) |  |  |  |  | 4.0 |  |  |
| Percent Blockage |  |  |  |  | 2 |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |
| Median type |  |  |  |  | None |  |  |
| Median storage veh) |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |
| vC, conflicting volume | 182 |  |  |  | 606 | 177 |  |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |
| vC 2 , stage 2 conf vol |  |  |  |  |  |  |  |
| vCu , unblocked vol | 182 |  |  |  | 606 | 177 |  |
| tC, single (s) | 4.1 |  |  |  | 6.4 | 6.2 |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |
| tF (s) | 2.2 |  |  |  | 3.5 | 3.3 |  |
| p0 queue free \% | 95 |  |  |  | 98 | 99 |  |
| cM capacity (veh/h) | 1373 |  |  |  | 431 | 853 |  |
| Direction, Lane \# | EB 1 | WB 1 | SW 1 |  |  |  |  |
| Volume Total | 360 | 164 | 16 |  |  |  |  |
| Volume Left | 68 | 0 | 10 |  |  |  |  |
| Volume Right | 0 | 8 | 5 |  |  |  |  |
| cSH | 1373 | 1700 | 516 |  |  |  |  |
| Volume to Capacity | 0.05 | 0.10 | 0.03 |  |  |  |  |
| Queue Length ( ft ) | 4 | 0 | 2 |  |  |  |  |
| Control Delay (s) | 1.8 | 0.0 | 12.2 |  |  |  |  |
| Lane LOS | A |  | B |  |  |  |  |
| Approach Delay (s) | 1.8 | 0.0 | 12.2 |  |  |  |  |
| Approach LOS |  |  | B |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 1.6 |  |  |  |  |
| Intersection Capacity Utilization |  |  | 43.3\% | ICU Level of Service |  |  | A |

HCM Unsignalized Intersection Capacity Analysis
16: Quackenbos Street \& New Hampshire Avenue


HCM Signalized Intersection Capacity Analysis
1: Peabody Street \& New Hampshire Avenue
07/07/2005

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | 4 |  |  | 4 |  |  | $4 \%$ |  |  | $4{ }^{4}$ |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  |  | 4.0 |  |  | 4.0 |  |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  |  | 0.95 |  |  | 0.95 |  |
| Frpb, ped/bikes |  | 0.99 |  |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Flpb, ped/bikes |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Frt |  | 0.96 |  |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Flt Protected |  | 0.99 |  |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Satd. Flow (prot) |  | 1755 |  |  | 1854 |  |  | 3527 |  |  | 3522 |  |
| Flt Permitted |  | 0.89 |  |  | 0.97 |  |  | 0.85 |  |  | 1.00 |  |
| Satd. Flow (perm) |  | 1573 |  |  | 1802 |  |  | 3006 |  |  | 3522 |  |
| Volume (vph) | 21 | 94 | 56 | 26 | 329 | 1 | 25 | 440 | 2 | 0 | 1188 | 32 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 22 | 97 | 58 | 27 | 339 | 1 | 26 | 454 | 2 | 0 | 1225 | 33 |
| Lane Group Flow (vph) | 0 | 177 | 0 | 0 | 367 | 0 | 0 | 482 | 0 | 0 | 1258 | 0 |
| Confl. Peds. (\#/hr) | 4 |  | 7 | 7 |  | 4 | 4 |  | 1 | 1 |  | 4 |
| Turn Type | Perm |  |  | Perm |  |  | Perm |  |  | Perm |  |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Actuated Green, G (s) |  | 25.0 |  |  | 25.0 |  |  | 65.0 |  |  | 65.0 |  |
| Effective Green, g (s) |  | 26.0 |  |  | 26.0 |  |  | 66.0 |  |  | 66.0 |  |
| Actuated g/C Ratio |  | 0.26 |  |  | 0.26 |  |  | 0.66 |  |  | 0.66 |  |
| Clearance Time (s) |  | 5.0 |  |  | 5.0 |  |  | 5.0 |  |  | 5.0 |  |
| Lane Grp Cap (vph) |  | 409 |  |  | 469 |  |  | 1984 |  |  | 2325 |  |
| v/s Ratio Prot |  |  |  |  |  |  |  |  |  |  | c0.36 |  |
| v/s Ratio Perm |  | 0.11 |  |  | c0.20 |  |  | 0.16 |  |  |  |  |
| $\mathrm{v} / \mathrm{c}$ Ratio |  | 0.43 |  |  | 0.78 |  |  | 0.24 |  |  | 0.54 |  |
| Uniform Delay, d1 |  | 30.9 |  |  | 34.4 |  |  | 6.9 |  |  | 9.0 |  |
| Progression Factor |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  | 0.20 |  |
| Incremental Delay, d2 |  | 3.3 |  |  | 12.3 |  |  | 0.3 |  |  | 0.6 |  |
| Delay (s) |  | 34.2 |  |  | 46.6 |  |  | 7.2 |  |  | 2.4 |  |
| Level of Service |  | C |  |  | D |  |  | A |  |  | A |  |
| Approach Delay (s) |  | 34.2 |  |  | 46.6 |  |  | 7.2 |  |  | 2.4 |  |
| Approach LOS |  | C |  |  | D |  |  | A |  |  | A |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: | :--- |
| HCM Average Control Delay | 13.0 | HCM Level of Service | B |
| HCM Volume to Capacity ratio | 0.61 |  | 8.0 |
| Cycle Length (s) | 100.0 | Sum of lost time (s) | C |
| Intersection Capacity Utilization | $74.0 \%$ | ICU Level of Service |  |
| C Critical Lane Group |  |  | A |

HCM Signalized Intersection Capacity Analysis
2: Rittenhouse Street \& New Hampshire Avenue

|  |  | $\rightarrow$ | T |  | 㐋 |  |  | 4 | 4 | $p$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | EBR2 | WBL2 | WBL | WBT | WBR | NBT | NBR | SBL2 | SBL |
| Lane Configurations |  | ¢ |  |  |  |  | 4 |  | 4 A |  |  | \% |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 |  |  |  |  | 4.0 |  | 4.0 |  |  | 4.0 |
| Lane Util. Factor |  | 1.00 |  |  |  |  | 1.00 |  | 0.95 |  |  | 1.00 |
| Frpb, ped/bikes |  | 0.99 |  |  |  |  | 1.00 |  | 1.00 |  |  | 1.00 |
| Flpb, ped/bikes |  | 0.99 |  |  |  |  | 0.97 |  | 1.00 |  |  | 1.00 |
| Frt |  | 0.98 |  |  | 2 |  | 1.00 |  | 0.99 |  |  | 1.00 |
| Flt Protected |  | 0.97 |  |  |  |  | 0.97 |  | 1.00 |  |  | 0.95 |
| Satd. Flow (prot) |  | 1745 |  |  |  |  | 1760 |  | 3494 |  |  | 1770 |
| Flt Permitted |  | 0.82 |  |  |  |  | 0.82 |  | 1.00 |  |  | 0.95 |
| Satd. Flow (perm) |  | 1473 |  | - | 30 |  | 1487 |  | 3494 |  |  | 1770 |
| Volume (vph) | 15 | 5 | 2 | 1 | 16 | 89 | 89 | 1 | 489 | 35 | 3 | 12 |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Adj. Flow (vph) | 16 | 5 | 2 | 1 | 17 | 96 | 96 | 1 | 526 | 38 | 3 | 13 |
| Lane Group Flow (vph) | 0 | 24 | 0 | 0 | 0 | 0 | 210 | 0 | 564 | 0 | 0 | 16 |
| Confl. Peds. (\#/hr) | 10 |  | 13 | 13 | 13 | 13 |  | 10 |  | 14 | 14 | 14 |
| Turn Type | Perm |  |  |  | Perm | Perm |  |  |  |  | Prot | Prot |
| Protected Phases |  | 4 |  |  |  |  | 8 |  |  |  | 14 | 14 |
| Permitted Phases | 4 |  |  |  | 8 | 8 |  |  | 2 |  |  |  |
| Actuated Green, G (s) |  | 27.0 |  |  |  |  | 27.0 |  | 44.0 |  |  | 14.0 |
| Effective Green, g (s) |  | 28.0 |  |  |  |  | 28.0 |  | 45.0 |  |  | 15.0 |
| Actuated g/C Ratio |  | 0.28 |  |  |  |  | 0.28 |  | 0.45 |  |  | 0.15 |
| Clearance Time (s) |  | 5.0 |  |  |  |  | 5.0 |  | 5.0 |  |  | +5.0 |
| Lane Grp Cap (vph) |  | 412 |  |  |  |  | 416 |  | 1572 |  |  | 266 |
| v/s Ratio Prot |  |  |  |  |  |  |  |  |  |  |  | 0.01 |
| v/s Ratio Perm |  | 0.02 |  |  |  |  | c0.14 |  | 0.16 |  |  |  |
| v/c-Ratio |  | 0.06 |  |  |  |  | 0.50 |  | 0.36 |  |  | 0.06 |
| Uniform Delay, d1 |  | 26.3 |  |  |  |  | 30.2 |  | 18.0 |  |  | 36.5 |
| Progression Factor |  | 1.00 |  |  |  |  | 1.00 |  | 0.89 |  |  | 1.00 |
| Incremental Delay, d2 |  | 0.3 |  |  |  |  | 4.3 |  | 0.6 |  |  | 0.4 |
| Delay (s) |  | 26.6 |  |  |  |  | 34.5 |  | 16.6 |  |  | 36.9 |
| Level of Service |  | C |  |  |  |  | C |  | B |  |  | D |
| Approach Delay (s) |  | 26.6 |  |  |  | . | 34.5 |  | 16.6 |  |  |  |
| Approach LOS |  | C |  |  |  |  | C |  | B |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 17.5 |  | HCM Lev | el of S | rvice |  | B |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.67 |  |  |  |  |  |  |  |  |  |
| Cycle Length (s) |  |  | 100.0 |  | Sum of lo | st time |  |  | 8.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 87.6\% |  | CU Leve | of Se | vice |  | D |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

Total Future - AM

HCM Signalized Intersection Capacity Analysis
2: Rittenhouse Street \& New Hampshire Avenue


HCM Unsignalized Intersection Capacity Analysis
5: Peabody Street \& First Street
07/07/2005

|  |  |  |  |  |  |  |  | $\uparrow$ |  |  | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 |  |  | $\dagger$ |  |  | 4 |  |  | 4 |  |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  | , | 0\% |  |  | 0\% |  |
| Volume (veh/h) | 3 | 170 | 1 | 1 | 379 | 8 | 20 | 3 | 3 | 16 | 3 |  |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Hourly flow rate (veh/h) | 3 | 177 | 1 | 1 | 395 | 8 | 21 | 3 | 3 | 17 | 3 |  |
| Pedestrians |  | 2 |  |  |  |  |  | 1 |  |  |  |  |
| Lane Width (ft) |  | 12.0 |  |  |  |  |  | 12.0 |  |  |  |  |
| Walking Speed (ft/s) |  | 4.0 |  |  |  | 20 |  | 4.0 |  |  |  |  |
| Percent Blockage |  | 0 |  |  |  |  |  | 0 |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  | 312 |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  | 噱 |  |  |  |  |  |  |
| vC , conflicting volume | 403 |  |  | 179 |  |  | 592 | 590 | 179 | 590 | 586 | 401 |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu, unblocked vol | 403 |  |  | 179 |  | m | 592 | 590 | 179 | 590 | 586 | 401 |
| tC , single (s) | 4.1 |  |  | 4.1 |  |  | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 2.2 |  |  | 2.2 |  |  | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| po queue free \% | 100 |  |  | 100 |  |  | 95 | 99 | 100 | 96 | 99 | 100 |
| CM capacity (veh/h) | 1156 |  |  | 1395 |  |  | 412 | 418 | 864 | 414 | 420 | 648 |
| Direction, Lane \# | EB 1 | WB 1 | NB 1 | SB 1 |  |  |  |  |  |  |  |  |
| Volume Total | 181 | 404 | 27 | 22 |  |  |  |  |  |  |  |  |
| Volume Left | 3 | 1 | 21 | 17 |  |  |  |  |  |  |  |  |
| Volume Right | 1 | 8 | 3 | 2 |  |  |  |  |  |  |  |  |
| cSH | 1156 | 1395 | 439 | 430 |  |  |  |  |  |  |  |  |
| Volume to Capacity | 0.00 | 0.00 | 0.06 | 0.05 |  |  |  |  |  |  |  |  |
| Queue Length ( ft ) | 0 | 0 | 5 | 4 |  |  |  |  |  |  |  |  |
| Control Delay (s) | 0.2 | 0.0 | 13.7 | 13.8 |  |  |  |  |  |  |  |  |
| Lane LOS | A | A | B | B |  |  | 4 |  |  |  |  |  |
| Approach Delay (s) | 0.2 | 0.0 | 13.7 | 13.8 |  |  |  |  |  |  |  |  |
| Approach LOS |  |  | B | B |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 1.1 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Util | lization |  | 32.3\% | ICU Level of Service |  |  |  |  | A |  |  |  |

HCM Unsignalized Intersection Capacity Analysis
7: Peabody Street \&

|  |  |  |  |  | $\checkmark$ | 4 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | WBT | WBR | SEL | SER |  |  |
| Lane Configurations |  | $\uparrow$ | 今 |  | ${ }^{7}$ |  |  | F-3. |
| Sign Control |  | Free | Free |  | Stop |  |  |  |
| Grade |  | 0\% | 0\% |  | 0\% | \% |  | 3) |
| Volume (veh/h) | 2 | 5 | 6 | 355 | 131 | 5 |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |  | Sery |
| Hourly flow rate (veh/h) | 2 | 5 | 7 | 386 | 142 | 5 |  |  |
| Pedestrians |  |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |  |
| Walking Speed (ft/s) |  |  |  |  | W6. |  |  | Wxex ${ }^{\text {a }}$ |
| Percent Blockage |  |  |  |  |  |  |  |  |
| Right furn flare (veh) |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  | None |  |  |  |
| Median storage veh) |  |  |  |  | * |  |  |  |
| Upstream signal (ft) |  |  | 569 |  |  |  |  |  |
| pX , platoon unblocked |  |  |  |  |  |  |  | सntis |
| vC, conflicting volume | 392 |  |  |  | 209 | 199 |  |  |
| VC1, stage 1 conf vol |  |  |  |  |  | 尞 |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  |  |  |
| VCu , unblocked vol | 392 |  |  |  |  | 199 |  |  |
| tc, single (s) | 4.1 |  |  |  | 6.4 | 6.2 |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |  |
| tF (s) | 2.2 |  |  |  | 3.5 | 3.3 |  |  |
| po queue free \% | 100 |  |  |  | 82 | 99 |  |  |
| cM capacity (veh/h) | 1166 |  |  |  | 778 | 842 |  |  |
| Direction, Lane\# | EB 1 | WB 1 | SE 1 |  |  |  |  |  |
| Volume Total | 8 | 392 | 148 |  |  |  |  |  |
| Volume Left | 2 | 0 | 142 |  |  |  |  |  |
| Volume Right | 0 | 386 | 5 |  |  |  |  |  |
| $\mathrm{CSH}^{\prime}$ | 1166 | 1700 | 780 |  |  |  |  |  |
| Volume to Capacity | 0.00 | 0.23 | 0.19 |  |  |  |  |  |
| Queue Length ( ft ) | 0 | 0 | 17 |  |  | \% |  |  |
| Control Delay (s) | 2.3 | 0.0 | 10.7 |  |  |  |  |  |
| LaneLOS | A |  | B |  |  | \% |  |  |
| Approach Delay (s) | 2.3 | 0.0 | 10.7 |  |  |  |  |  |
| Approach LOS |  |  | B |  |  | P |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 2.9 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 39.1\% | ICU Level of Service |  |  | A |  |

HCM Unsignalized Intersection Capacity Analysis
8: Rittenhouse Street \& Sligo Mill Road

|  | $\rightarrow$ | $\rightarrow$ | 2 | $\cdots$ | 4 | 1 | 3 | 7 | $\rho$ | 5 | * | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations |  |  |  |  | \& |  |  | ¢ |  |  | \& |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Stop |  |  | Stop |  |
| Volume (veh/h) | 0 | 0 | 0 | 20 | 138 | 6 | 4 | 9 | 14 | 8 | 9 | 16 |
| Peak Hour Factor | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 |
| Hourly flow rate (veh/h) | 0 | 0 | 0 | 24 | 164 | 7 | 5 | 11 | 17 | 10 | 11 | 19 |


| Direction, Lane \# | WB 1 | NE 1 | SW 1 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Volume Total (vph) | 195 | 32 | 39 |  |  |
| Volume Left (vph) | 24 | 5 | 10 |  |  |
| Volume Right (vph) | 7 | 17 | 19 |  |  |
| Hadj (s) | 0.0 | -0.2 | -0.2 |  |  |
| Departure Headway (s) | 4.1 | 4.1 | 4.1 |  |  |
| Degree Utilization, $x$ | 0.22 | 0.04 | 0.05 |  |  |
| Capacity (veh/h) | 865 | 834 | 833 |  |  |
| Control Delay (s) | 8.2 | 7.3 | 7.3 |  |  |
| Approach Delay (s) | 8.2 | 7.3 | 7.3 |  |  |
| Approach LOS | A | A | A |  |  |
| Intersection Summary |  |  |  |  |  |
| Delay |  |  | 8.0 |  |  |
| HCM Level of Service |  |  | A |  |  |
| Intersection Capacity Utilization |  |  | 26.0\% | ICU Level of Service | A |

